



Role of anisotropy during hydraulic fracturing true triaxial experiments in shales

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- University of Toronto -

ARMA Symposium 2025 - Large Block Hydraulic Fracturing in the Laboratory



GeologicAI

ShearFRAC[®]



with contributions by J. Ha, F. Nasser, M. Li, E. Magsipoc and P. Wu

- BSc. in Civil-Structural Engineering at Benha University, Cairo - Egypt (2007).
- About 10 years professional experience in Geotechnical Engineering (Laboratory and In-situ Testing/Instrumentation) in the United Arab Emirates.
- Joined Prof. Giovanni Grasselli Group at the University of Toronto in 2015 and earned my PhD. in 2023.
- About 12 peer-reviewed journal articles and 13 conference publications.
- Currently a Senior Completions Design and Geomechanics Engineer at Petronas Canada.

- Introduction
- Characterizing Anisotropy
- True Triaxial Sample Preparation and Test Procedure
- Results
- Findings
- Conclusions and Limitations

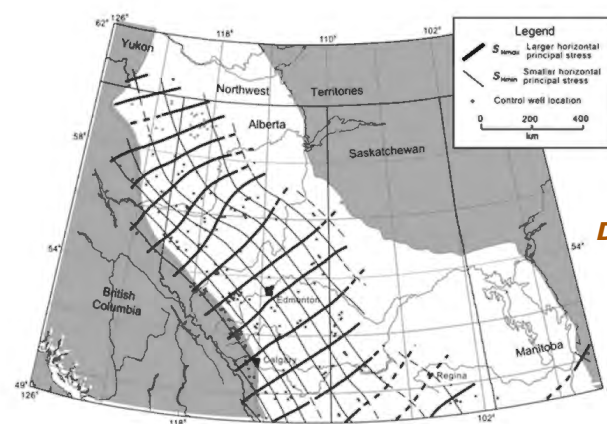


Image Source: Suarez-Rivera, R., et al. "Optimizing lateral landing depth for improved well production: Presented at the Unconventional Resources Technology Conference." URTeC-2460515 (2016).

The Montney Formation is the largest unconventional hydrocarbon play in Canada.

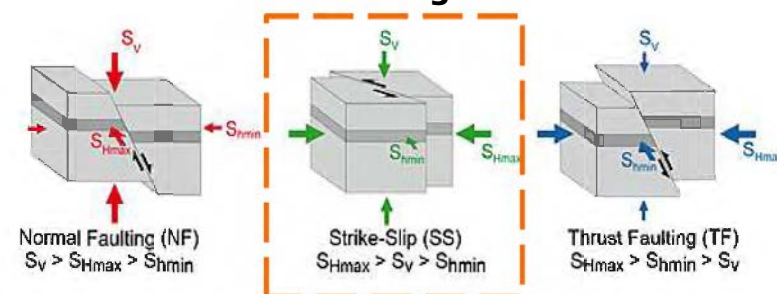
To date, there has been no studies on the hydromechanical characterization under true triaxial conditions for the Montney shale. In fact, these are non-existent for deep reservoirs.

There is very limited publicly available data for the mechanical properties of shale samples at depth. This is true for almost any fragile and water sensitive rock at depth.



**Extent of
Montney
Development**

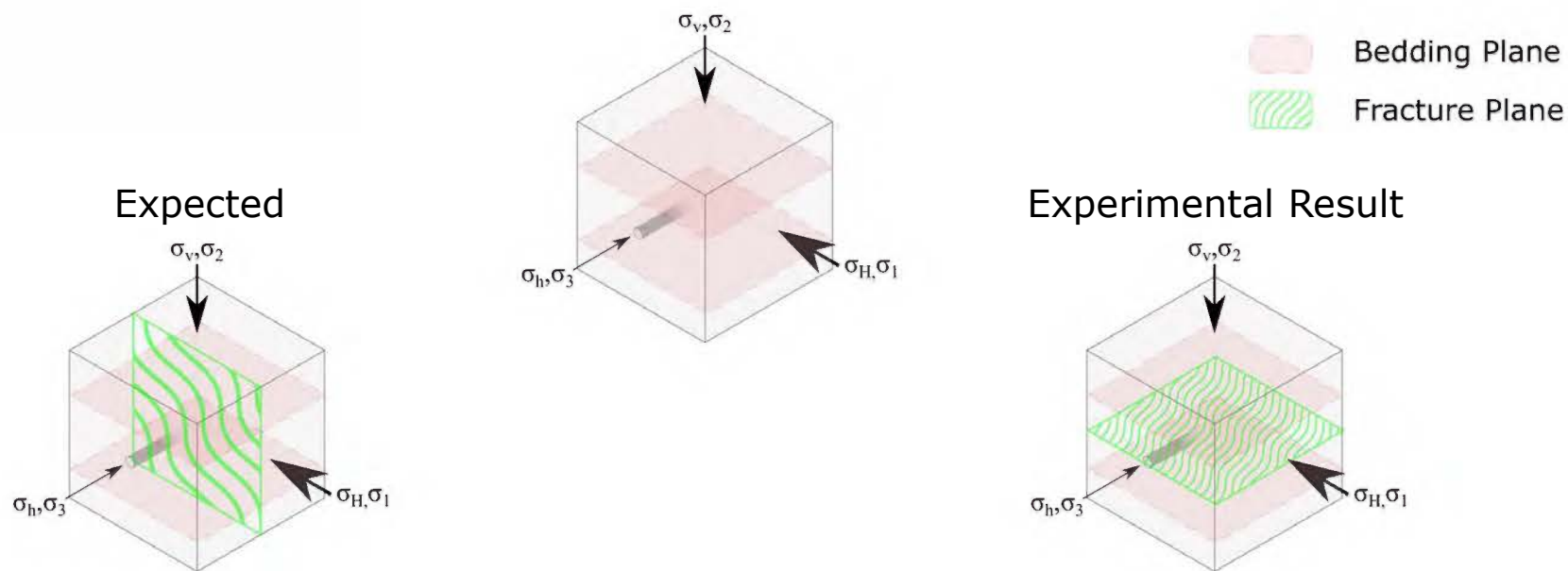
Stress Regimes



Source: <http://www.world-stress-map.org/data/>

Given a strike-slip stress regime, with a horizontal wellbore. The expected failure is against the least principal stress (σ_3).

Additionally, the fracture reopening pressure and the shut-in pressure are close to σ_3 .

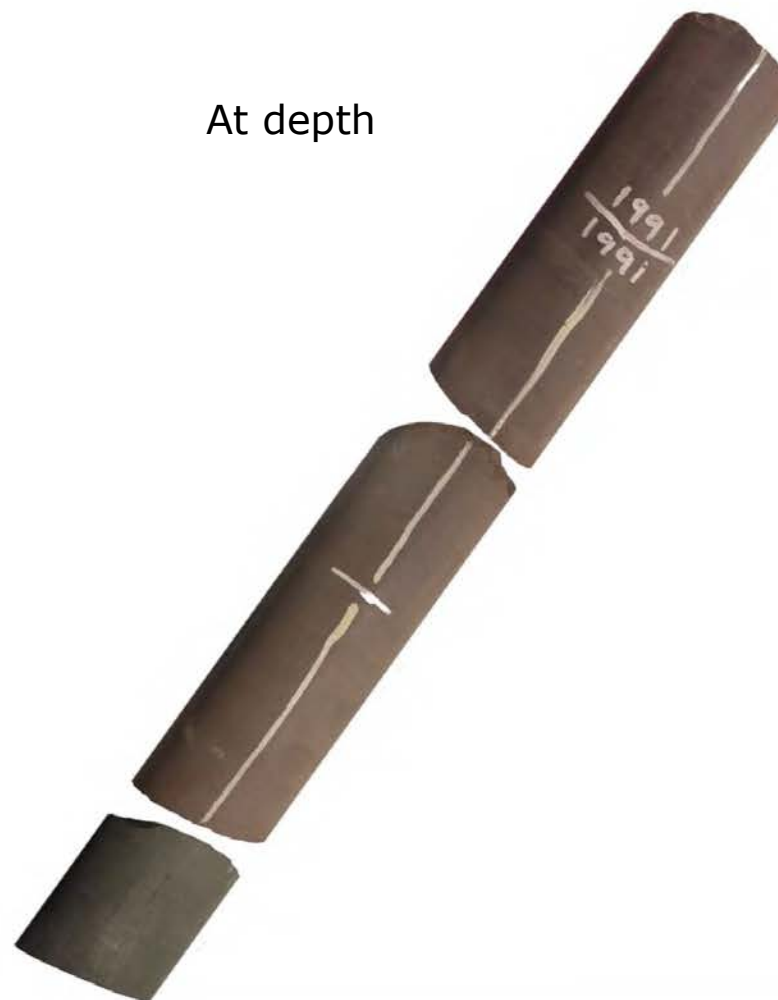


And can the shut-in pressure tell us more than just the magnitude of the principal stress.

Outcrop



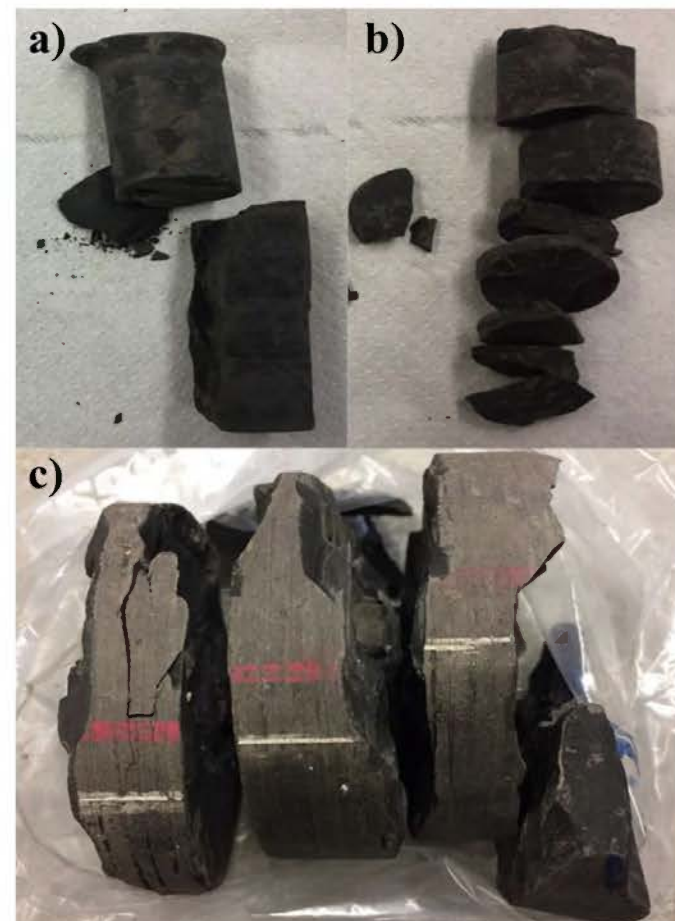
At depth

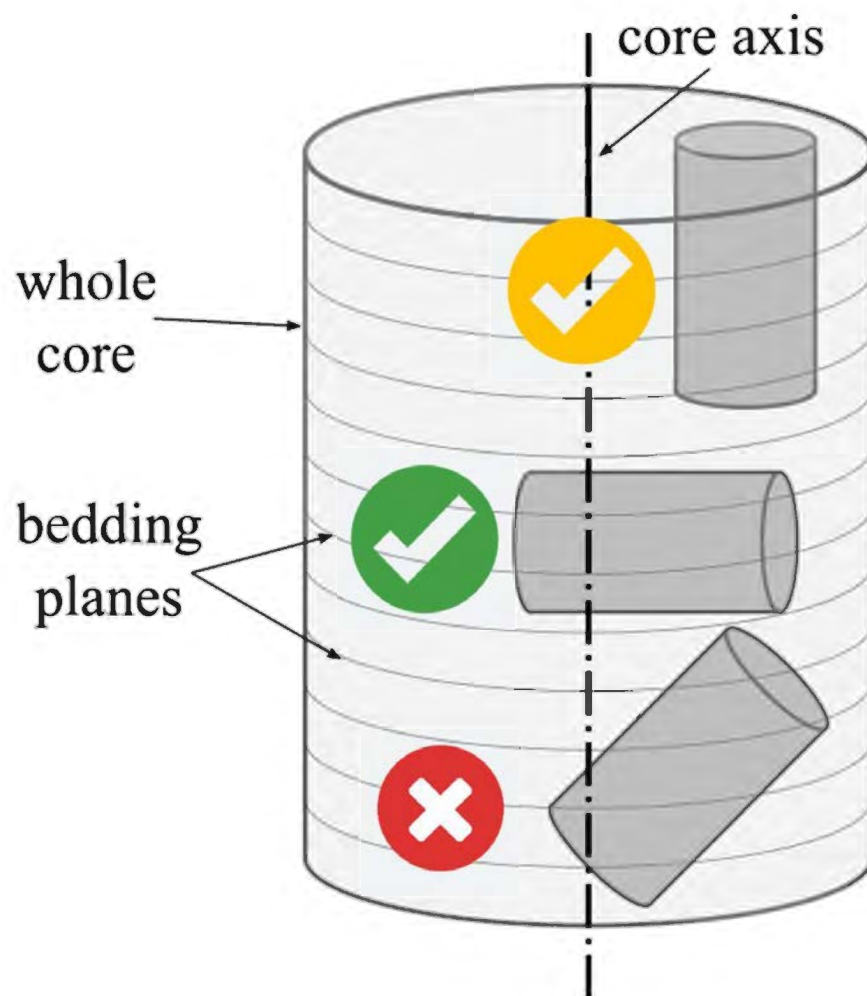


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Because of the unexpected results, we are now met with additional obstacles:

1. Limited laboratory testing due to difficulties arising from sampling procedures.
2. Absence of laboratory testing results that assess anisotropy.
3. Variability of the results for similar samples across testing laboratories and testing machines.





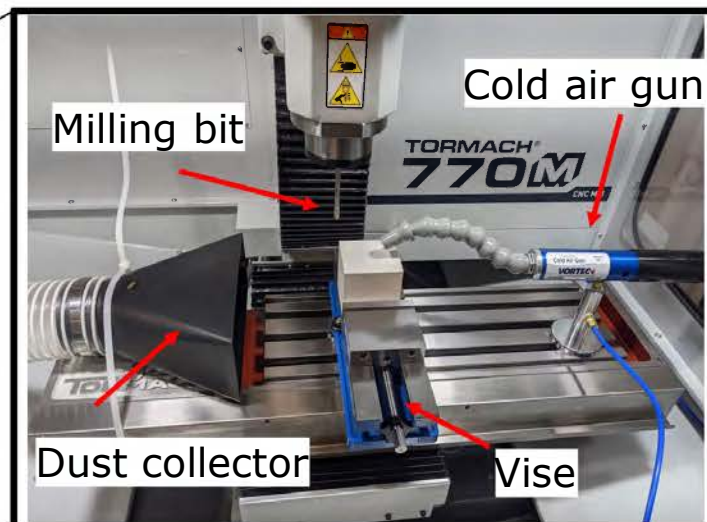
Perpendicular to bedding
Limited Success Rate

Parallel to bedding
High Success Rate

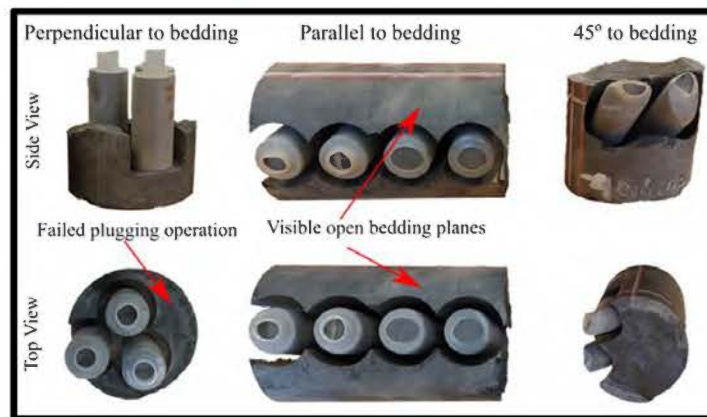
Angle to bedding
Rare Success



MILLFACE CLOSE-UP



TYPICAL RESULTS



Abdelaziz, A., Ha, J. & Grasselli, G. Novel Sub-core Extraction Method Using CNC Milling for Water-Sensitive and Fragile Rock. *Rock Mech Rock Eng* 57, 7683–7689 (2024). <https://doi.org/10.1007/s00603-024-03860-3>



Schematic of CNC Milling Operations

Parallel to core axis
Perpendicular to bedding

Side View



Failed plugging operation

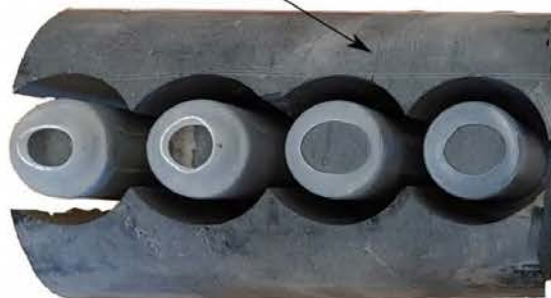
Top View



Perpendicular to core axis
Parallel to bedding

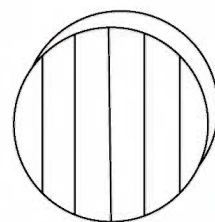
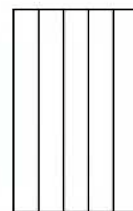
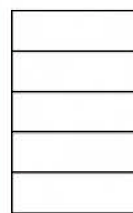


Visible open bedding planes



45° to core axis
45° to bedding





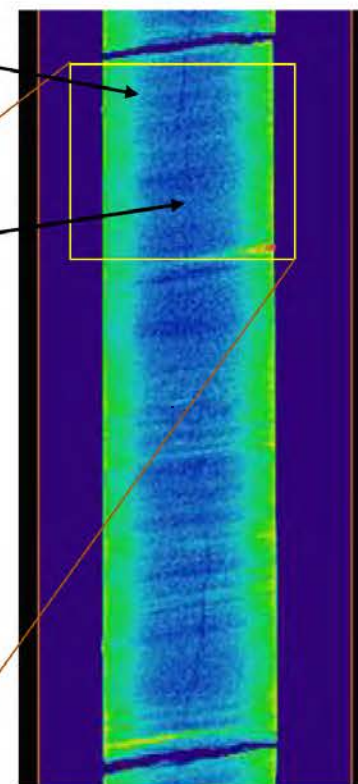
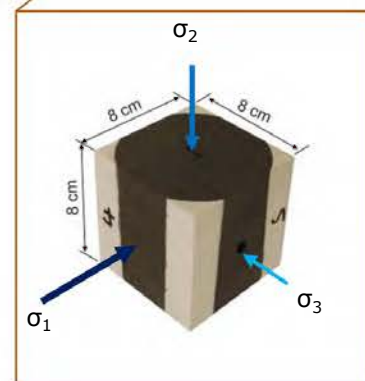
Example of Extracted Plugs

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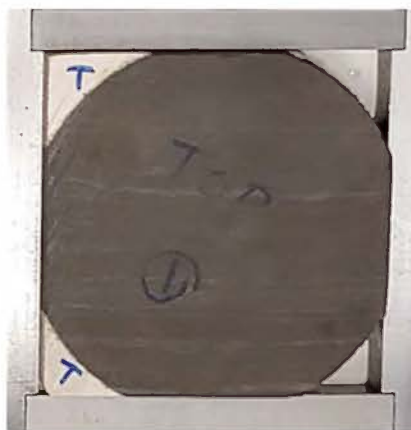
Opened bedding planes

Natural
fracture



Full-diameter core CT
(Provided by PETRONAS)

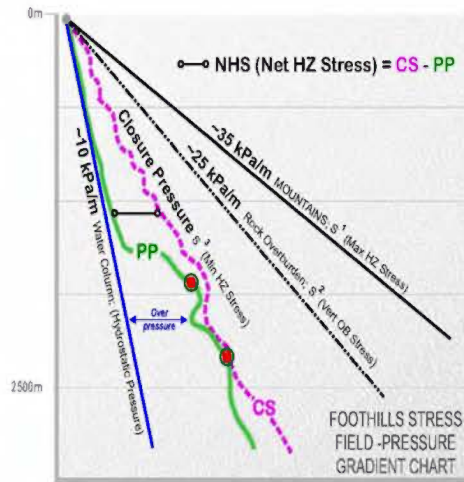
3D Rendering of the Core at Depth Sample



True Triaxial Tests – Sample Preparation

Input Parameters for True Triaxial Testing

Montney 1D MEM



Source: Khair and Adams 2019

- DFIT (Pore Pressure) Data Point
- Petrophysical Model: PP (Pore Pressure)*
- Petrophysical Model: CS (Closure Pressure)*

Reservoir Rock

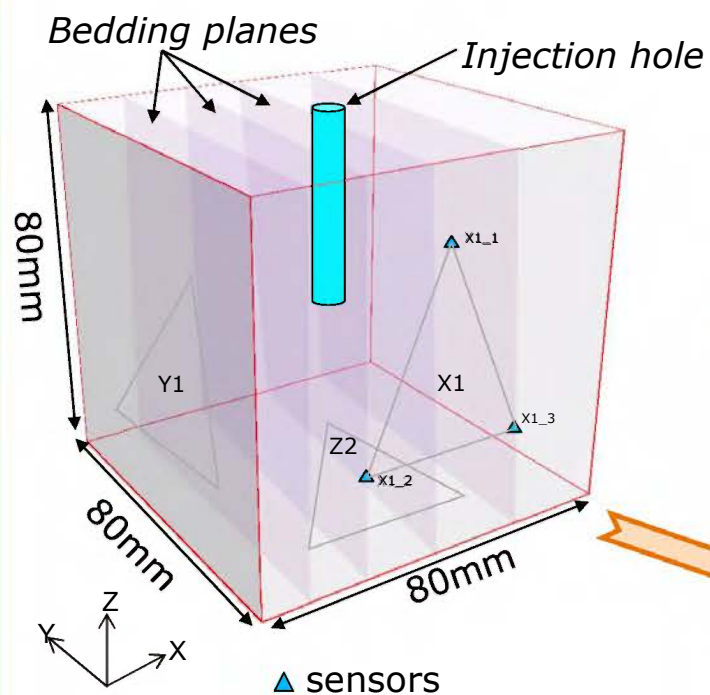


Injection Fluids

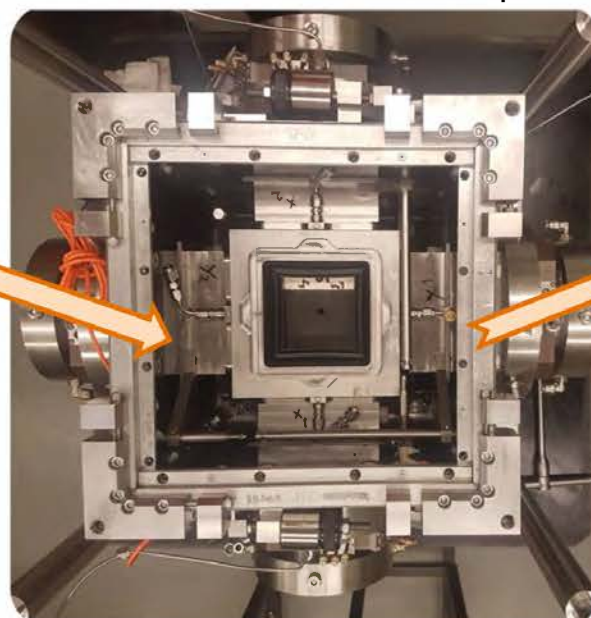
True Triaxial Testing Cell



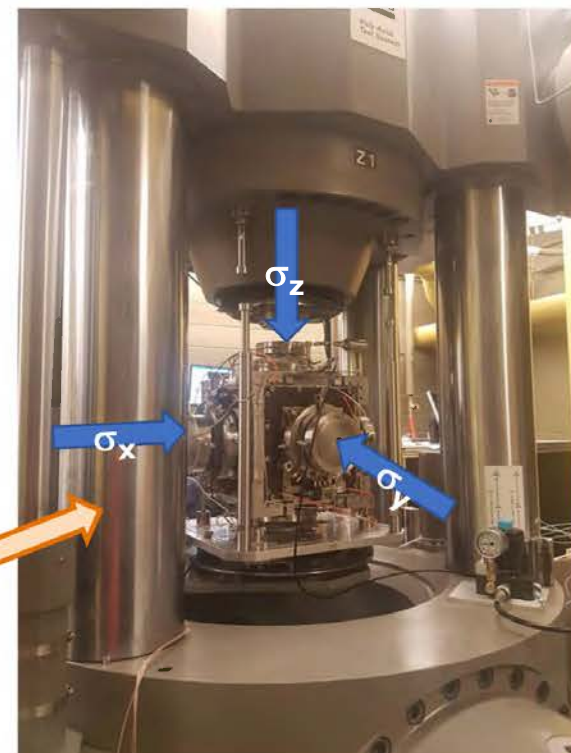
True principal stresses can be applied to the sample prior to hydraulic stimulation replicating reservoir stresses



- Independently applied $\sigma_1, \sigma_2, \sigma_3$
- 3 LVDT X,Y,Z directions
- 6 x 3 AE sensor
- 20 kHz – 1.2 MHz broad bandwidth resonant frequency

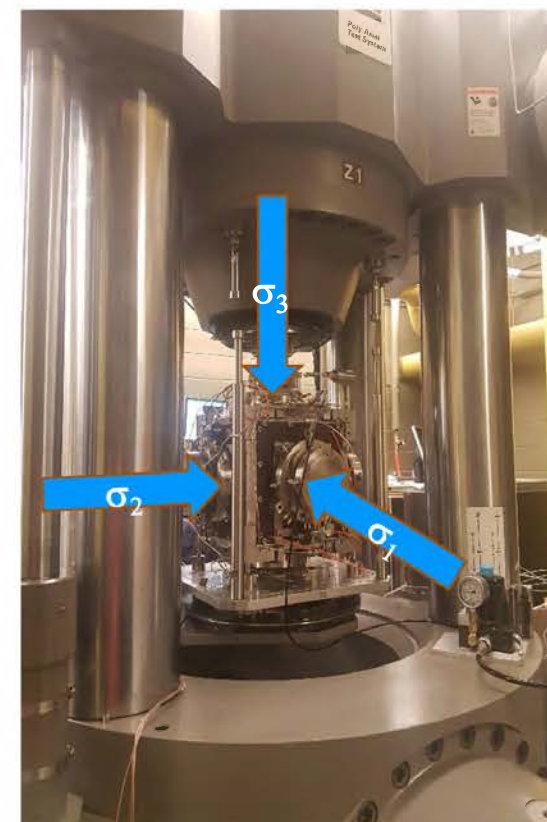
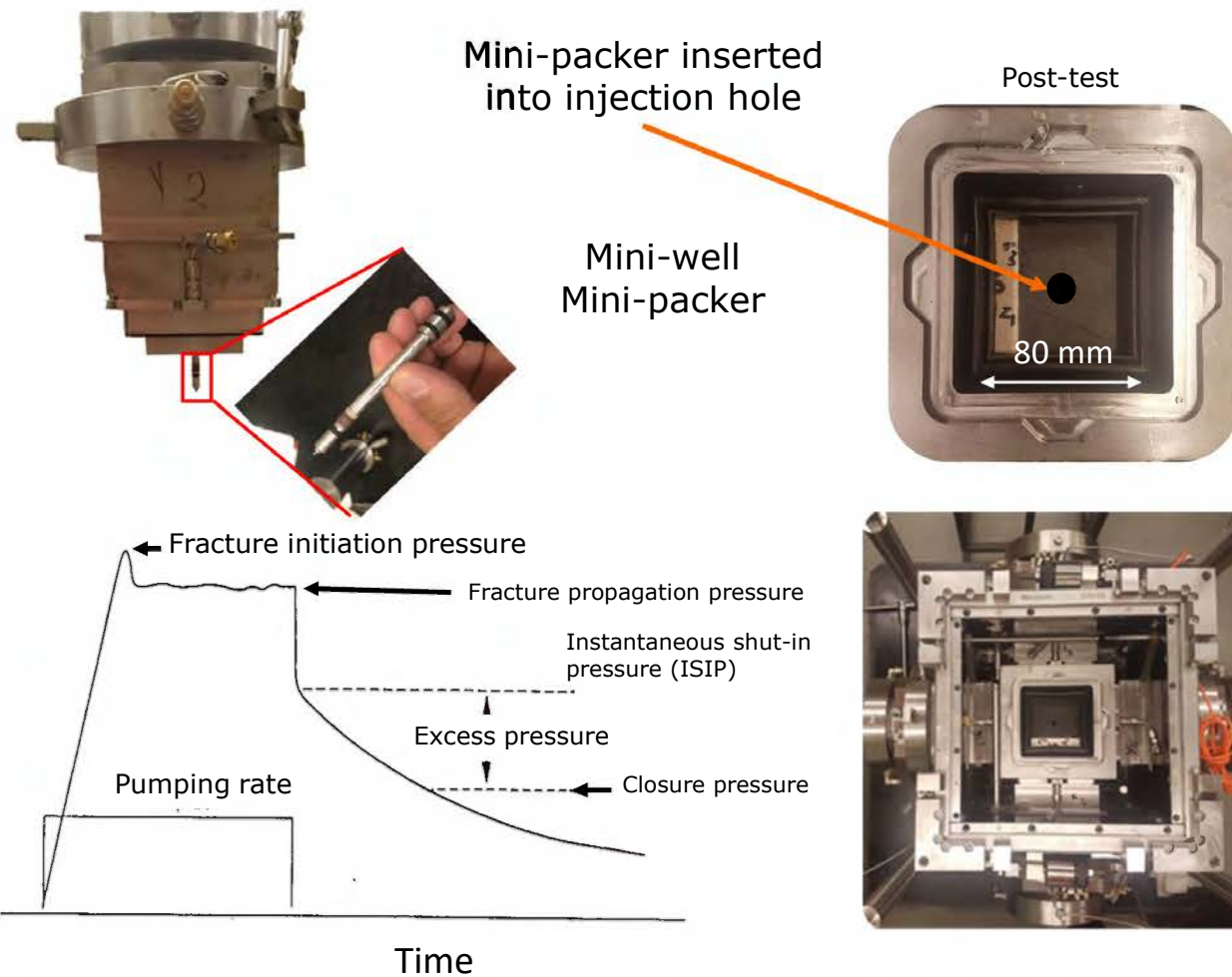


Test sample assembly
(Top view)



True triaxial (polyaxial) machine
(Side view)

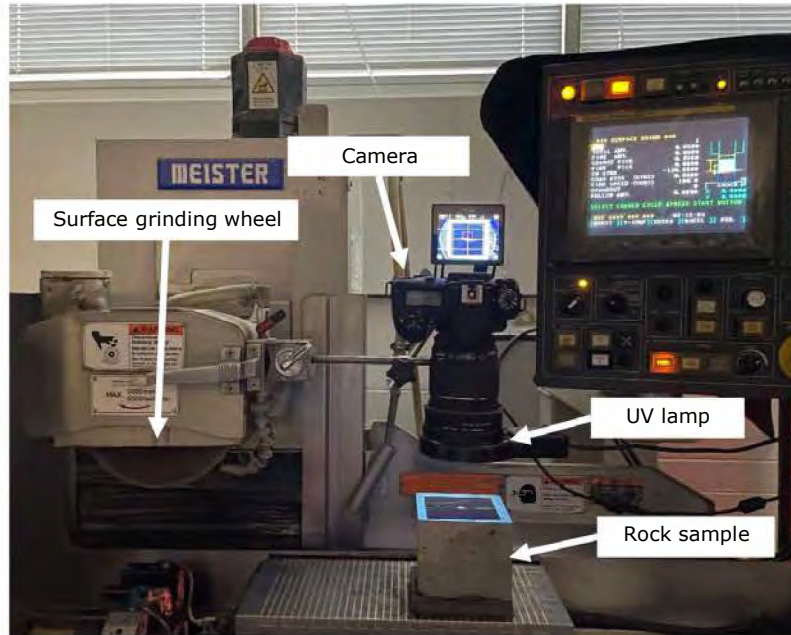
- 3-axes (X,Y,Z) 3-Comp (P,S1,S2) velocity survey
- Sampled at 10 MHz and 12-bit resolution



Polyaxial frame

Abdelaziz, A., Ha, J., Abul Khair, H., Adams, M., Tan, C. P., Musa, I. H., & Grasselli, G. (2019, September 23). Unconventional Shale Hydraulic Fracturing Under True Triaxial Laboratory Conditions, the Value of Understanding Your Reservoir. Society of Petroleum Engineers. doi:10.2118/196026-MS.

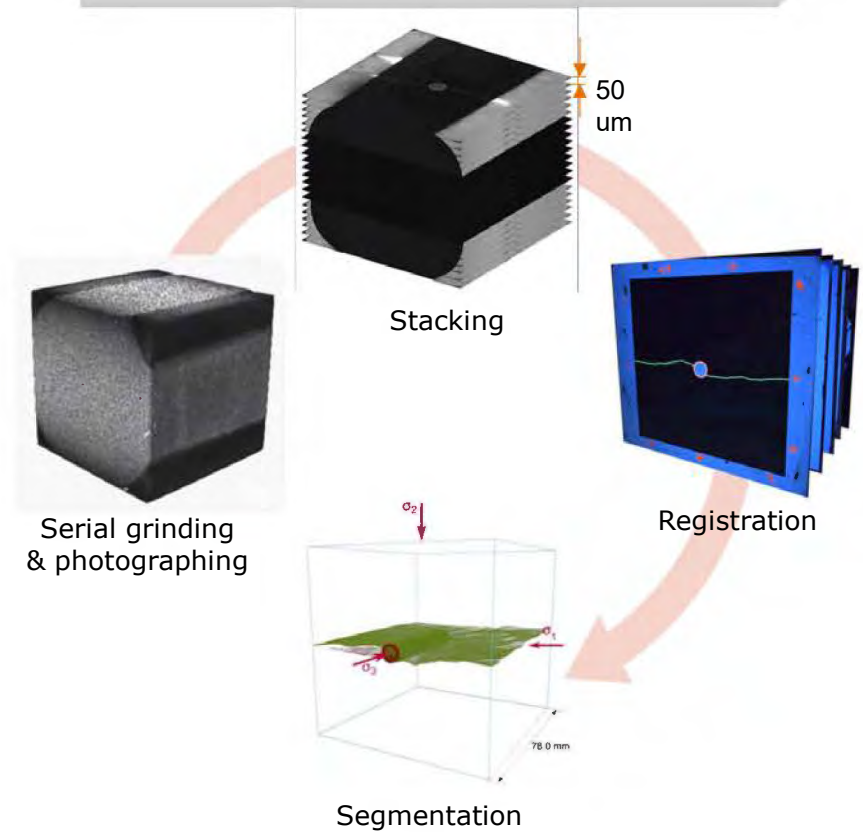
Experimental Setup



Sample size:
 $8 \times 8 \times 8 \text{ cm}^3$

Imaging Resolution:
 $26.5 \times 26.5 \times 50 \text{ } \mu\text{m}^3$

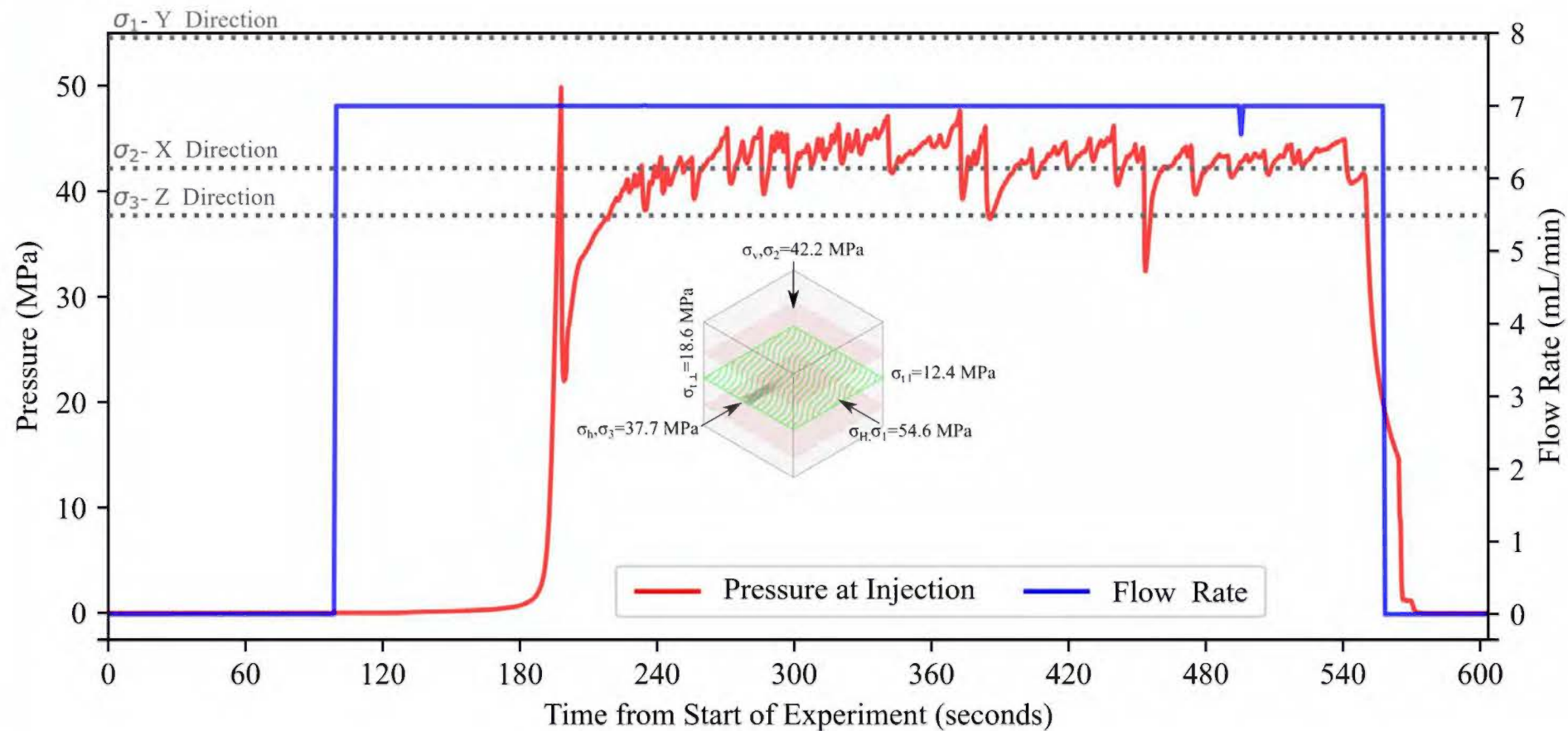
3D serial-sections reconstruction

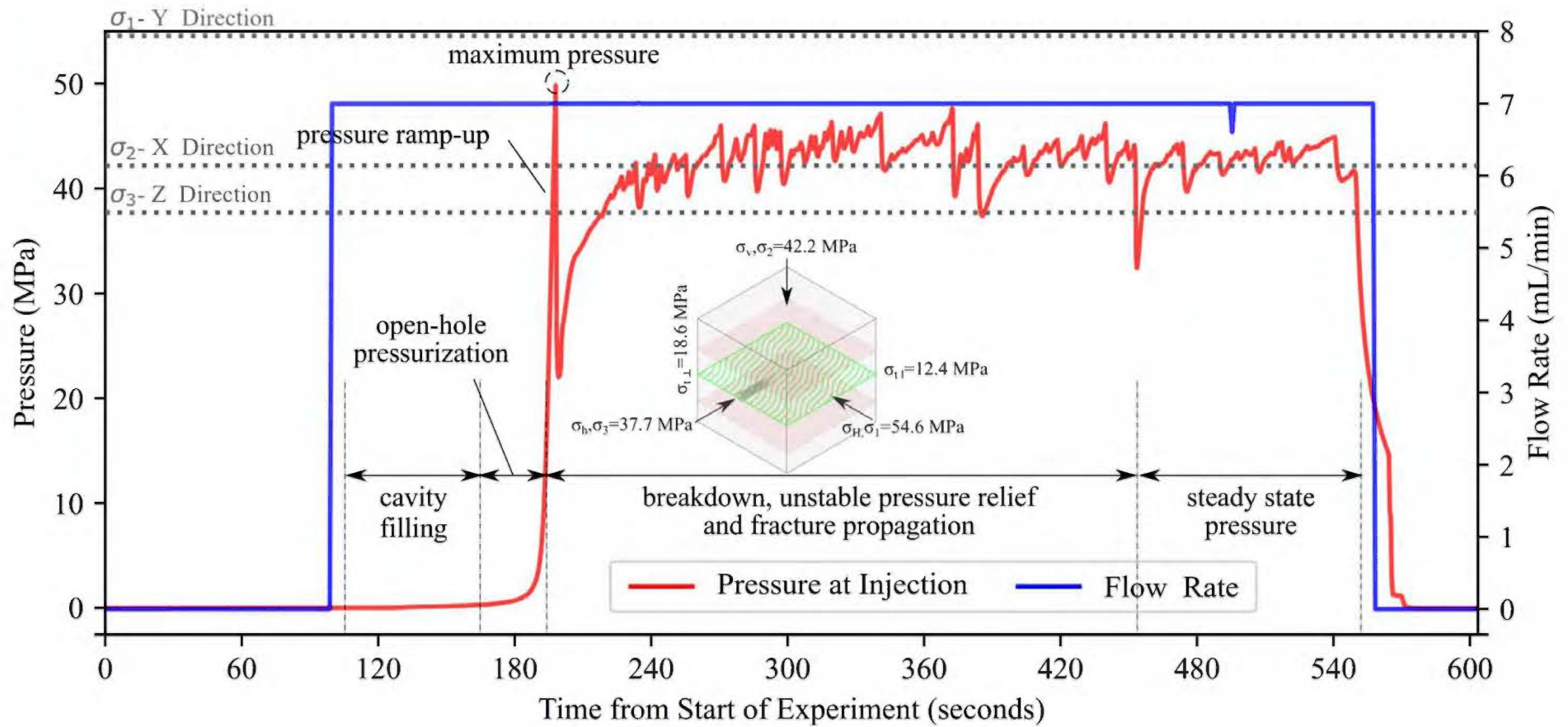


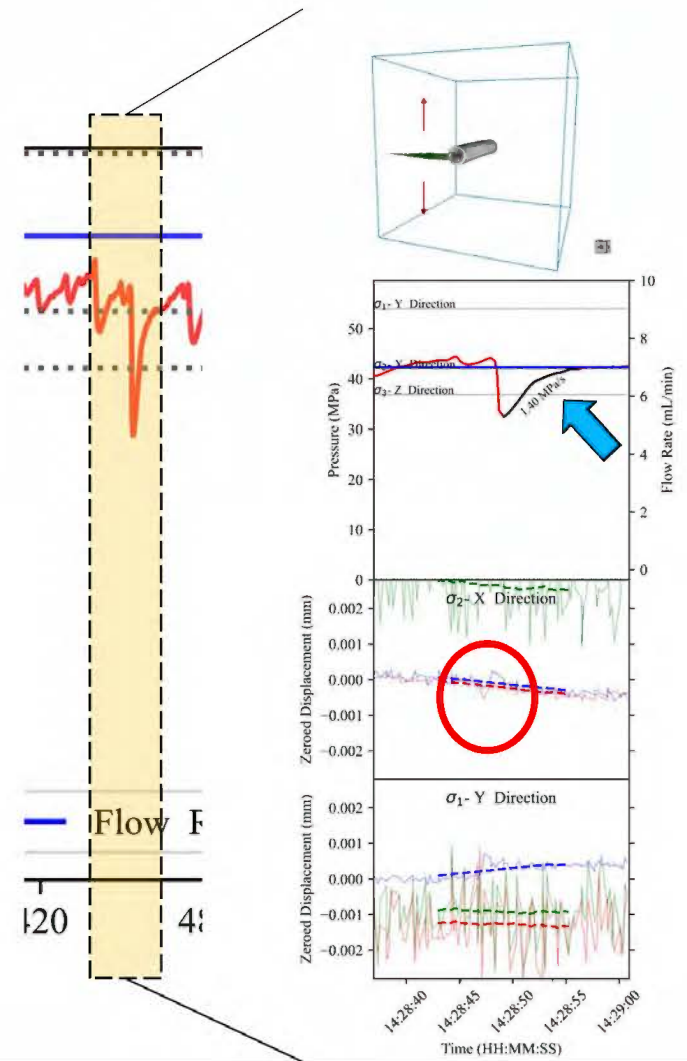
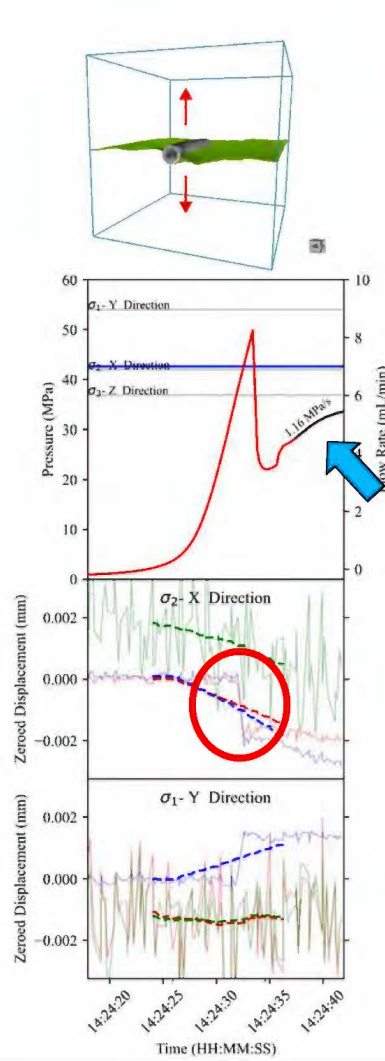
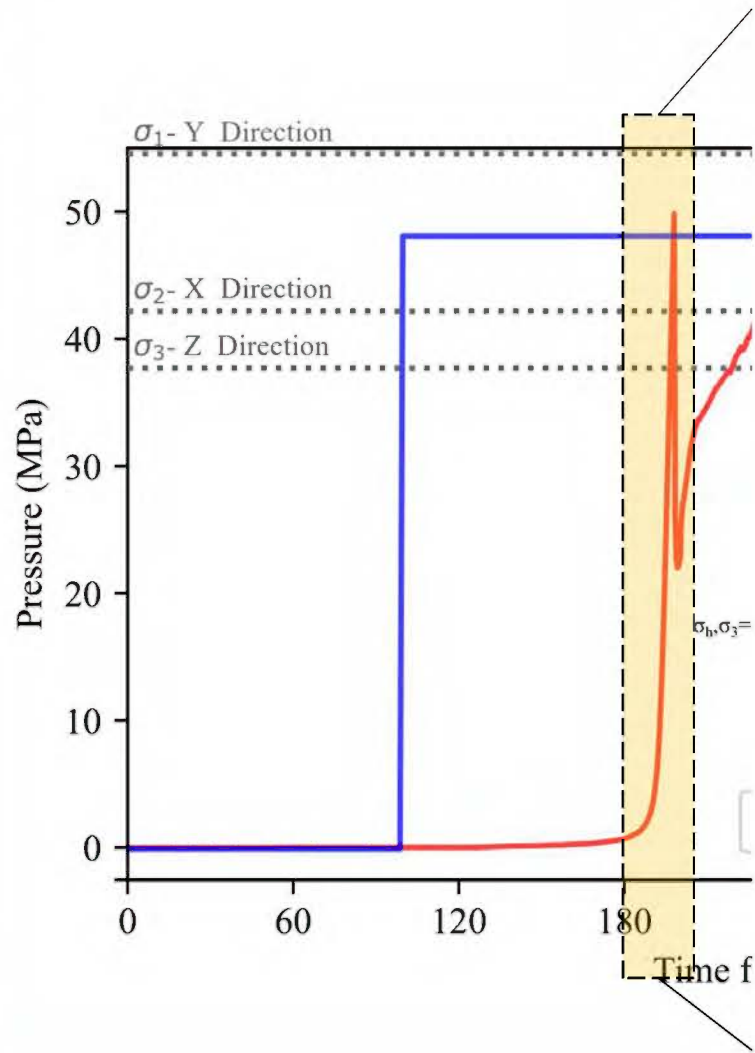
Li et al. "Mapping Fracture Complexity of Fractured Shale in Laboratory: Three-dimensional Reconstruction From Serial-section Images." *Rock Mechanics and Rock Engineering* (2021): 1-12.

Serial Sectioning

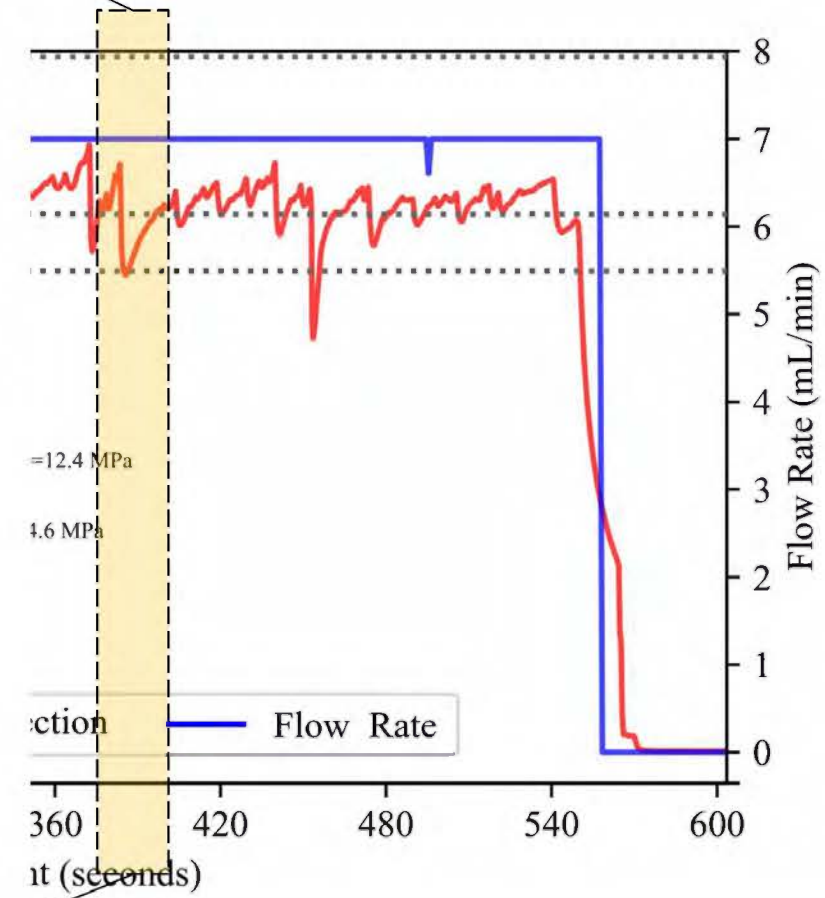
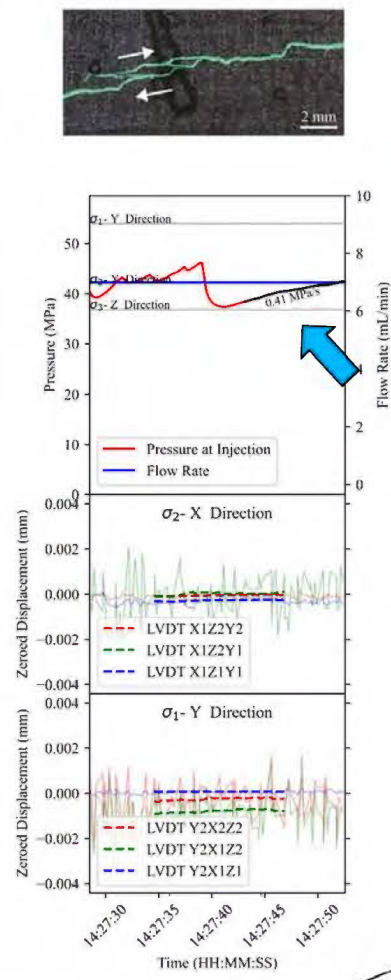
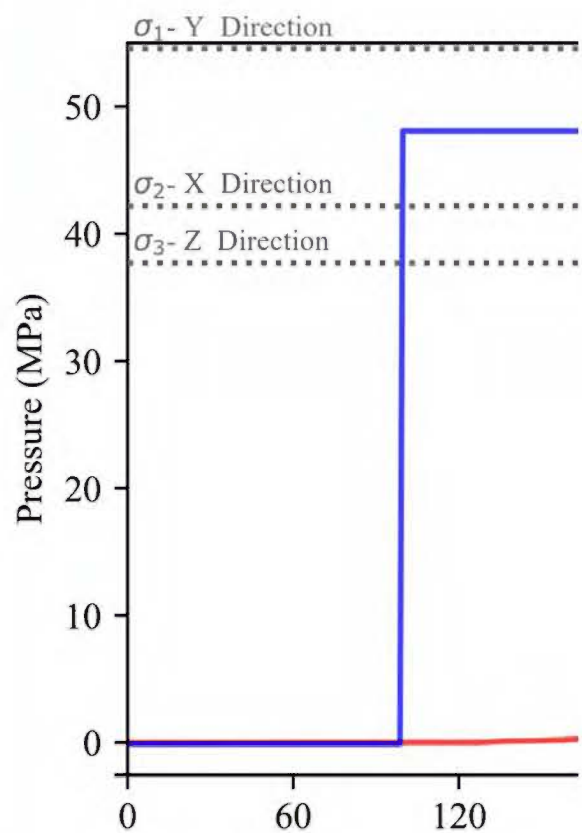
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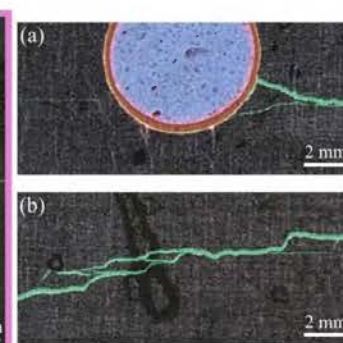
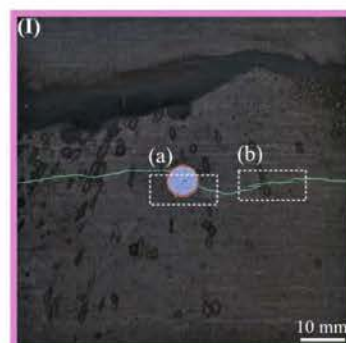
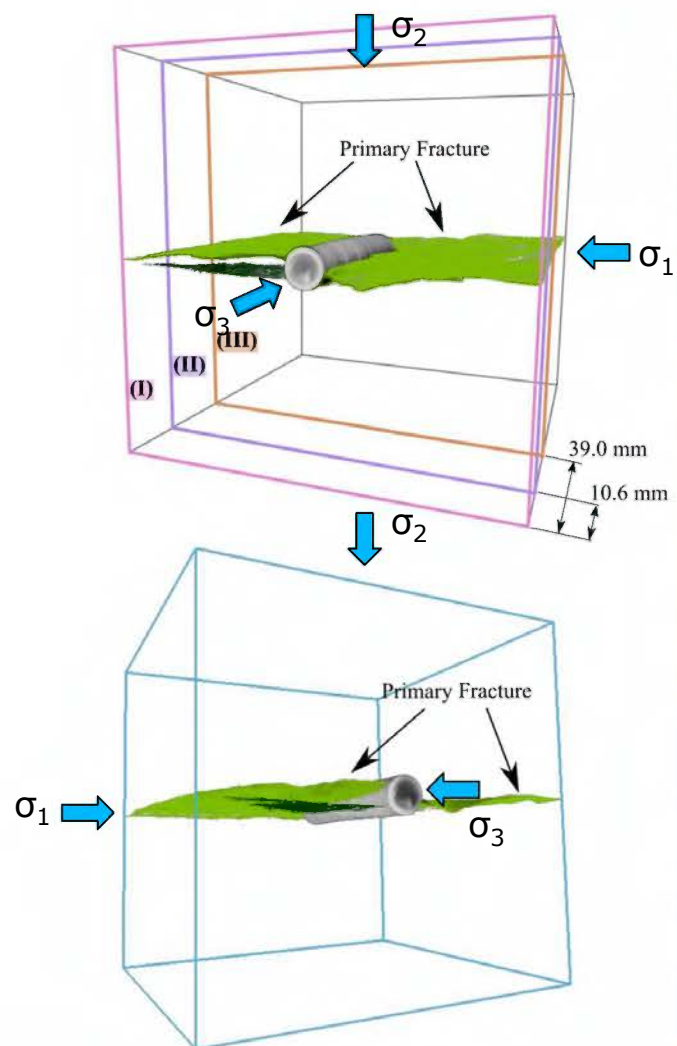


Outcrop Sample – Tensile Signature

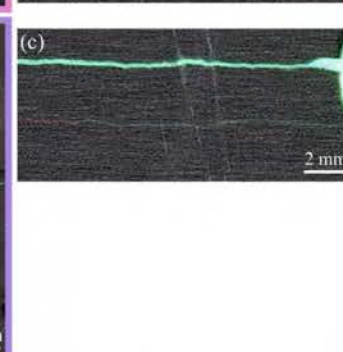
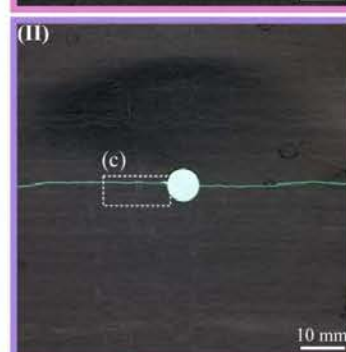


Outcrop Sample – Shear Signature

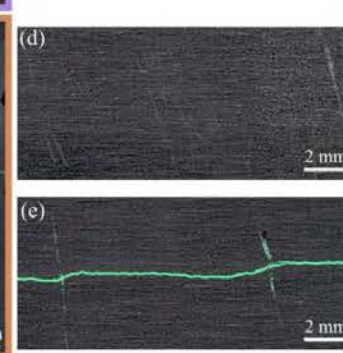
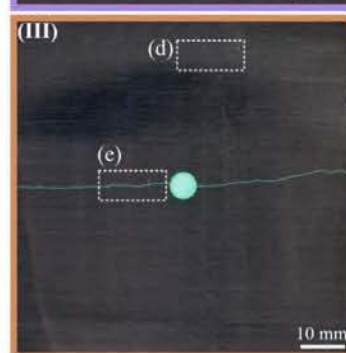




En-echelon



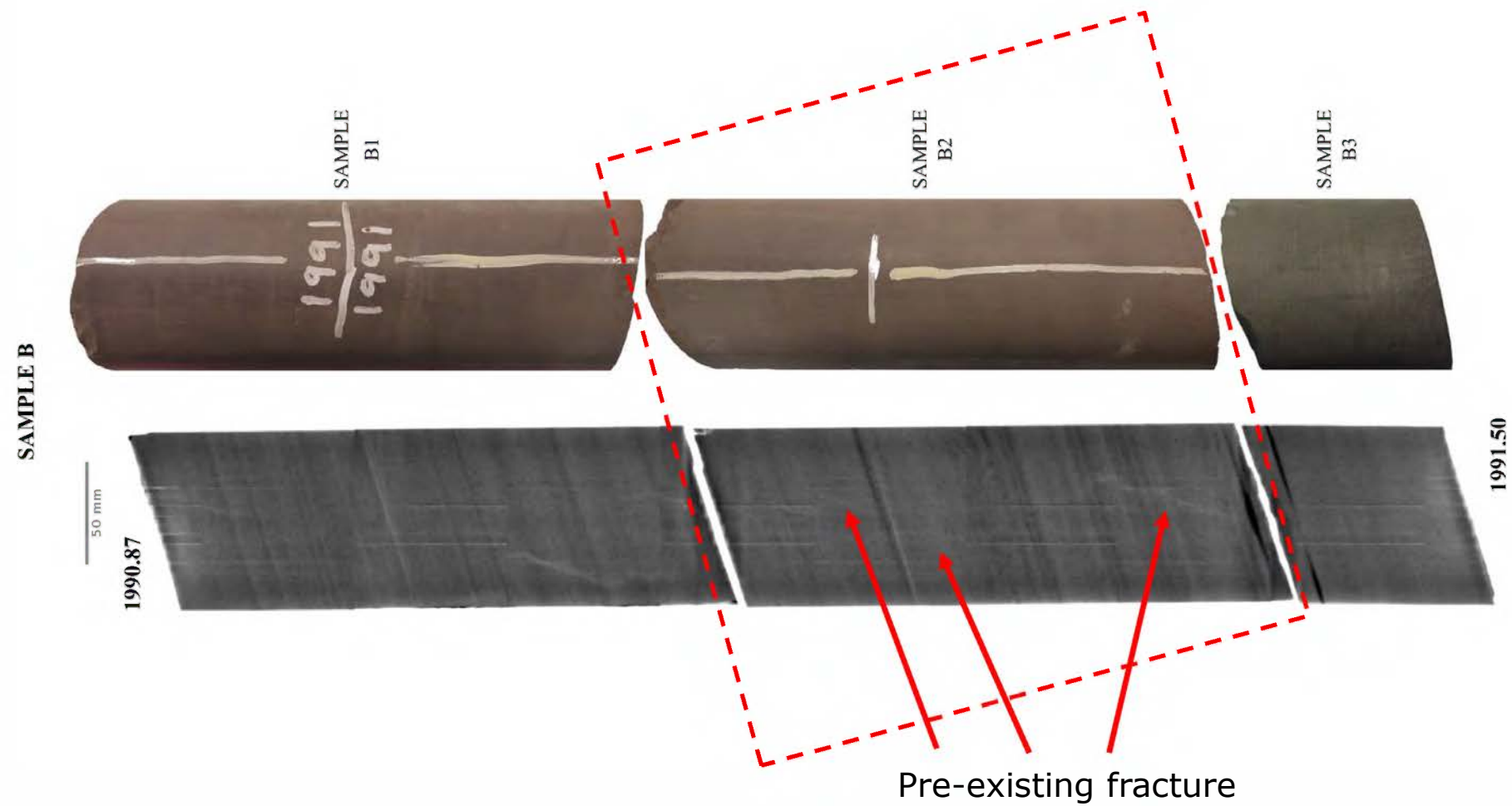
Horst and Graben



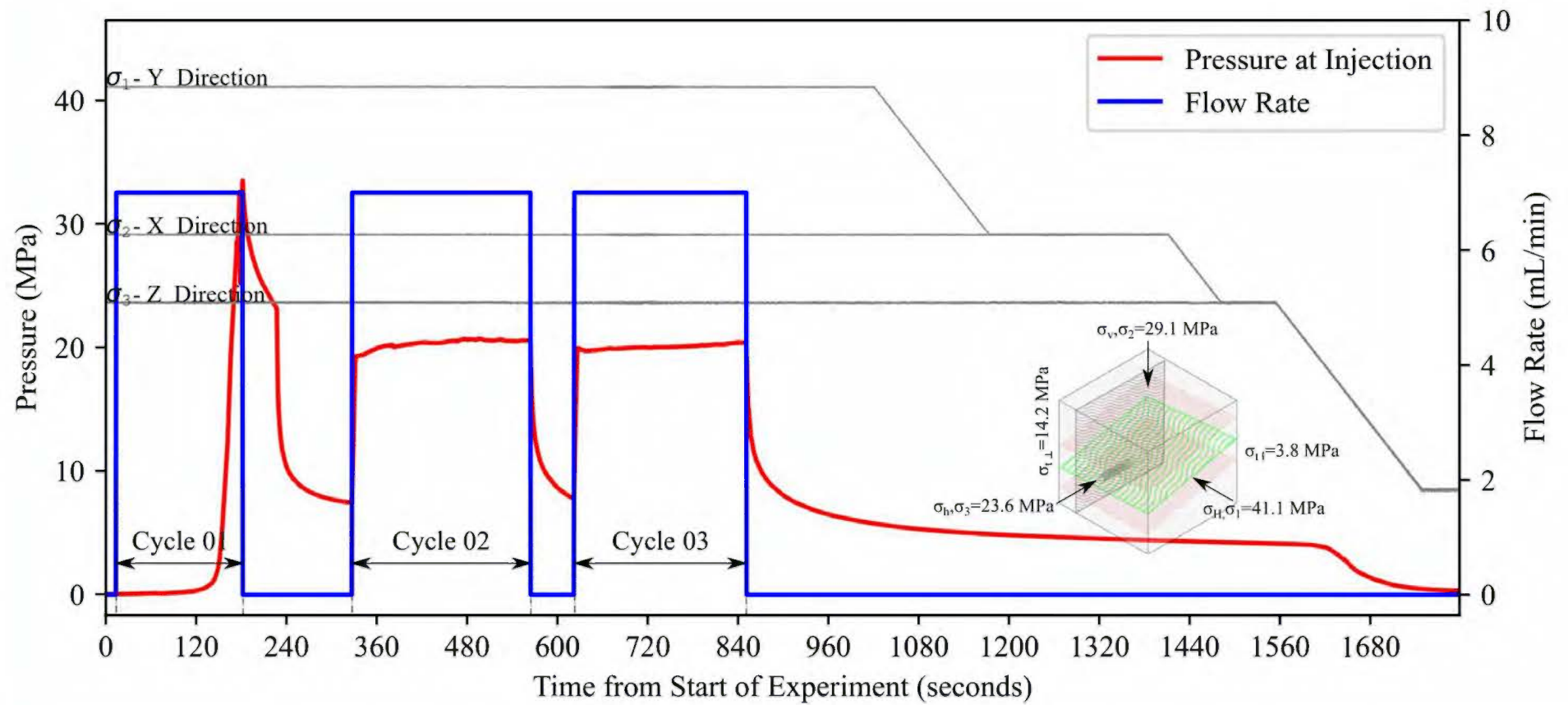
Horst and Graben

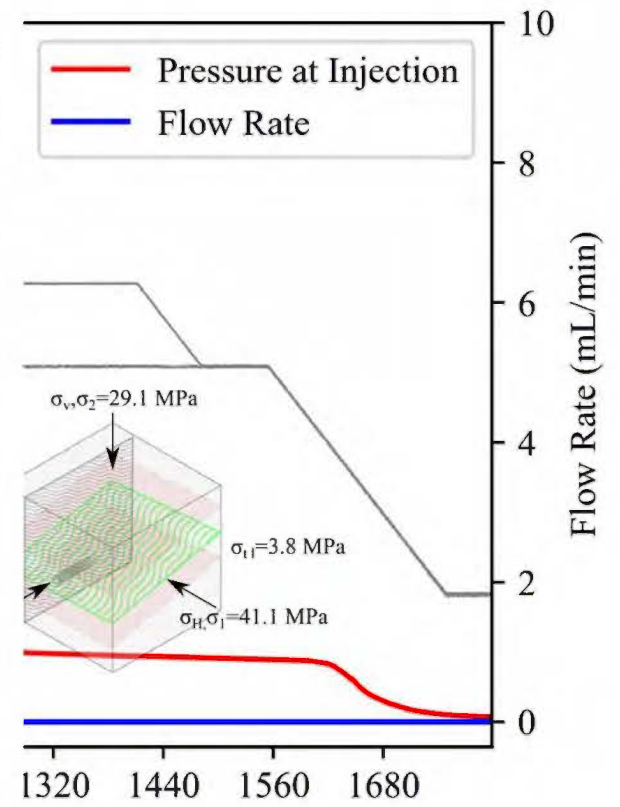
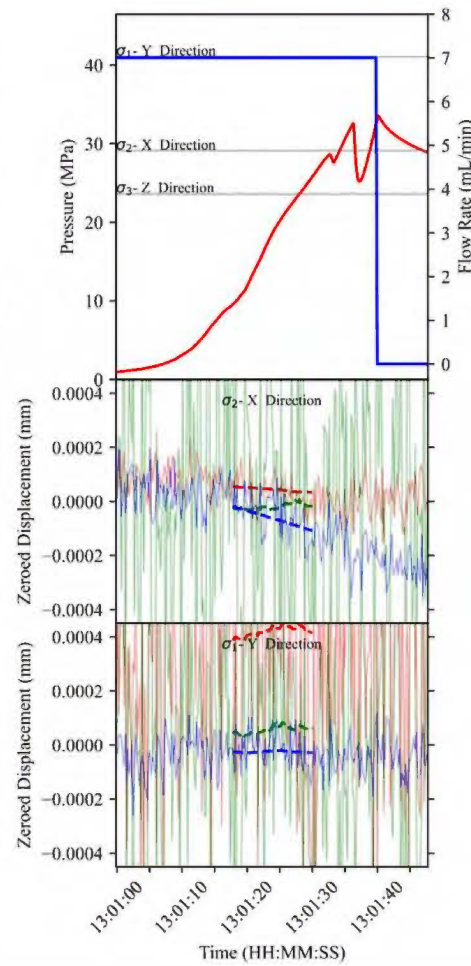
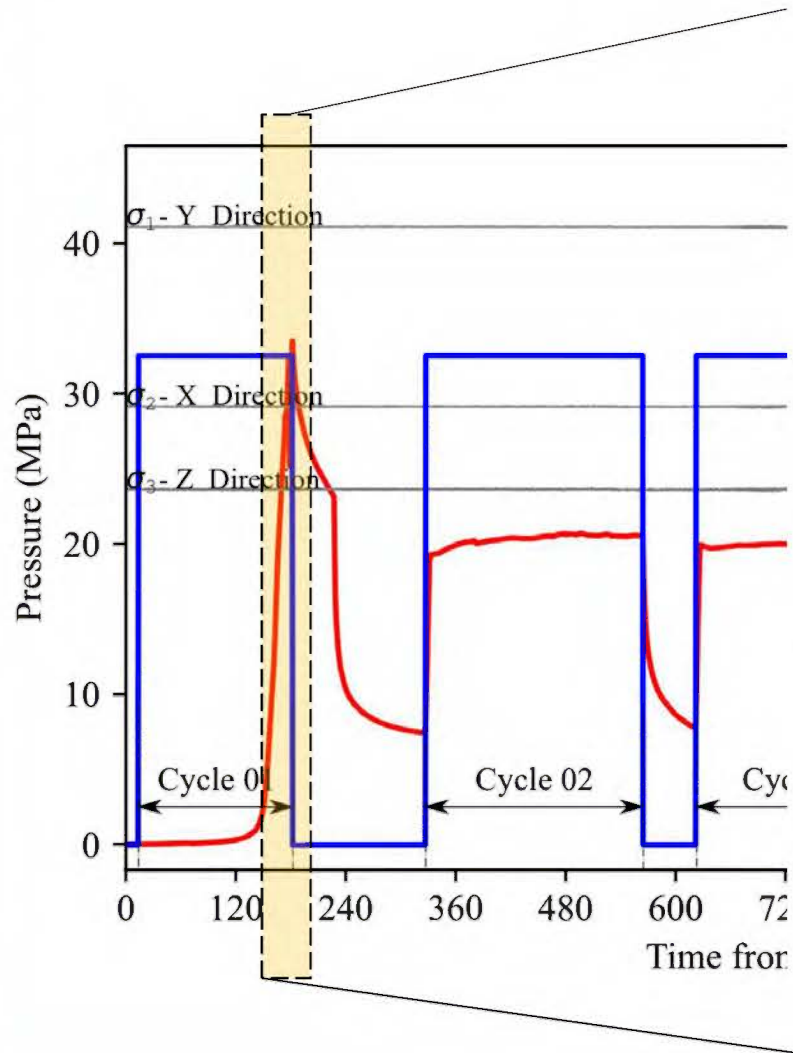


Outcrop Sample – Serial Sectioning Results

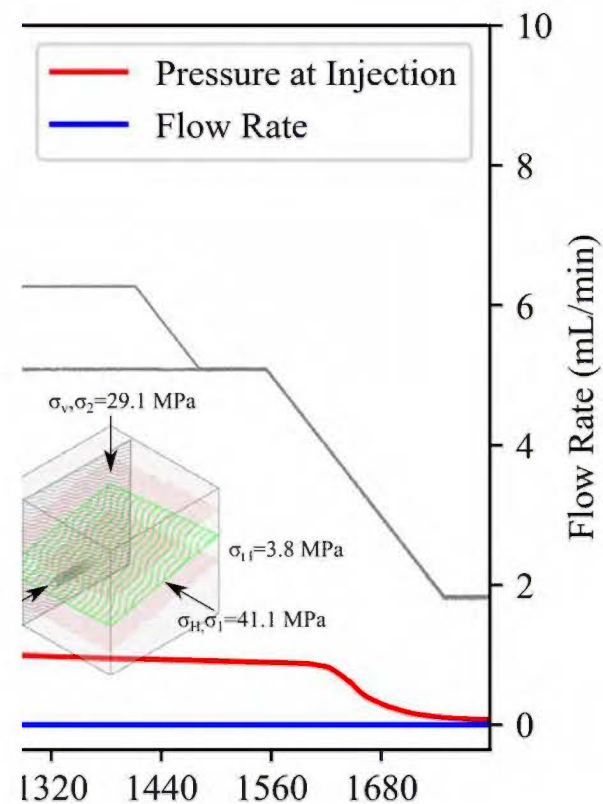
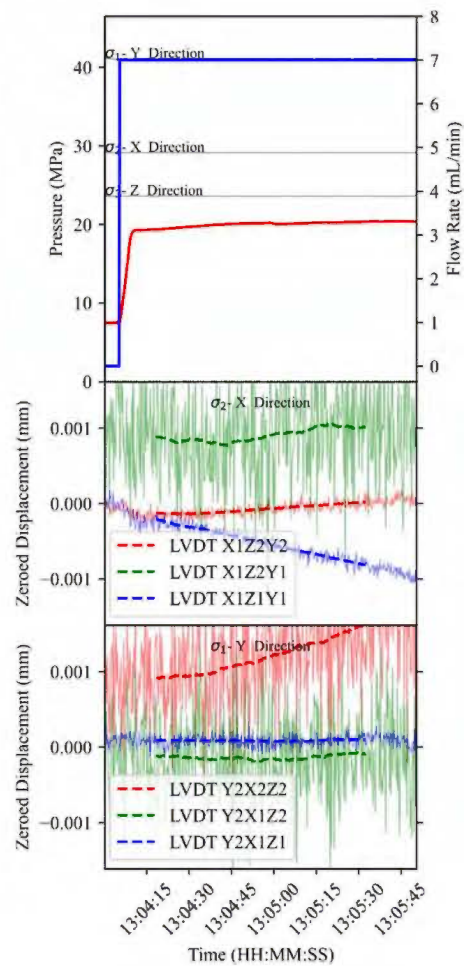
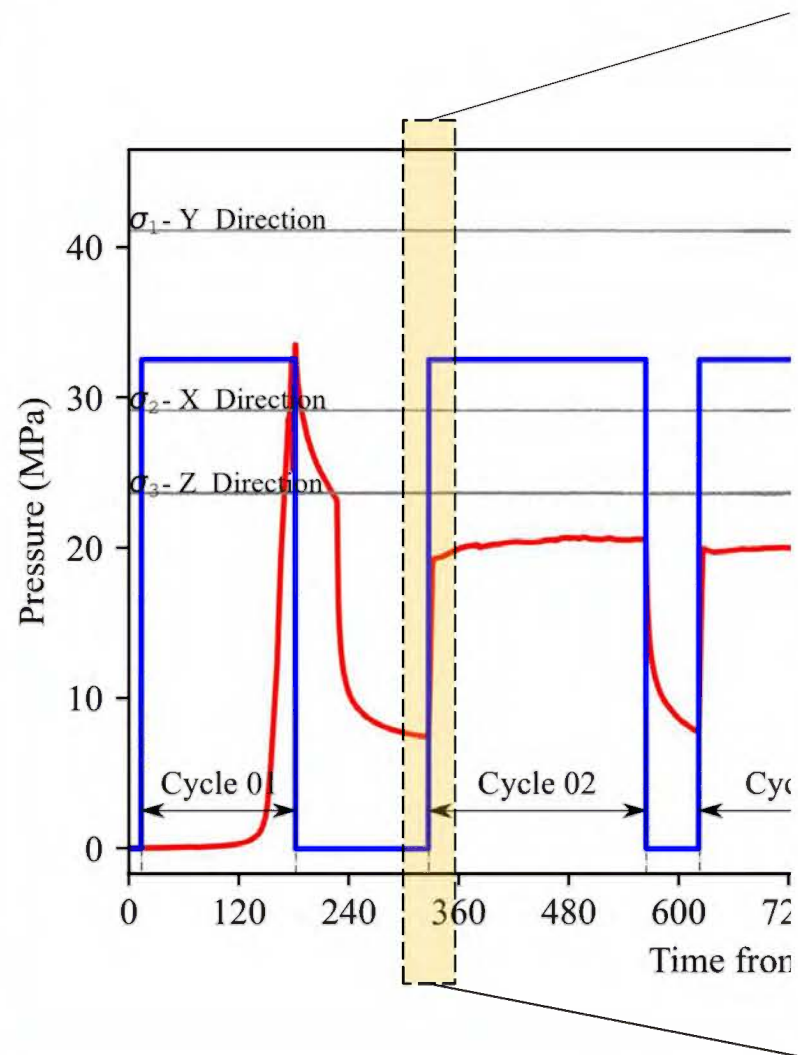


Whole Core Samples

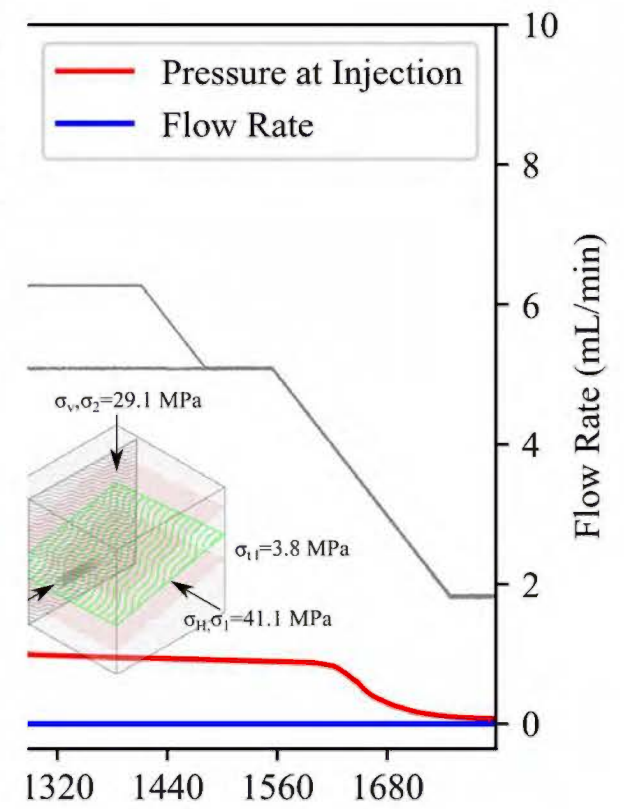
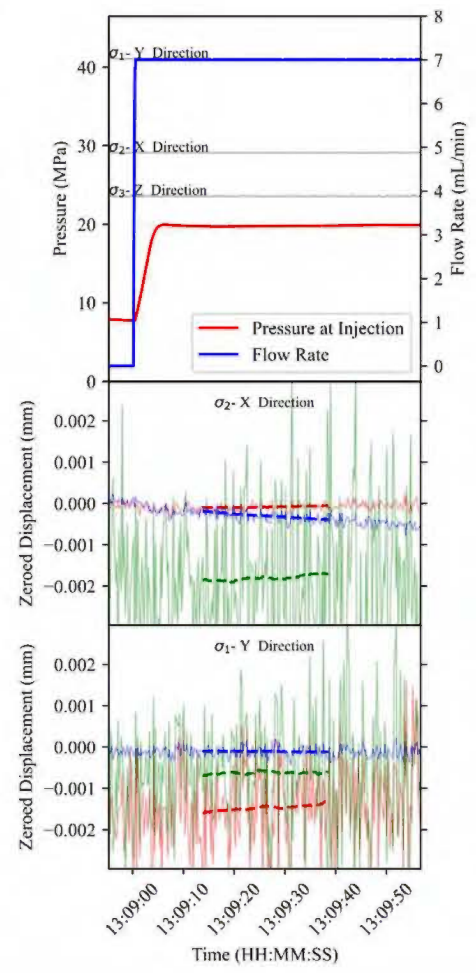
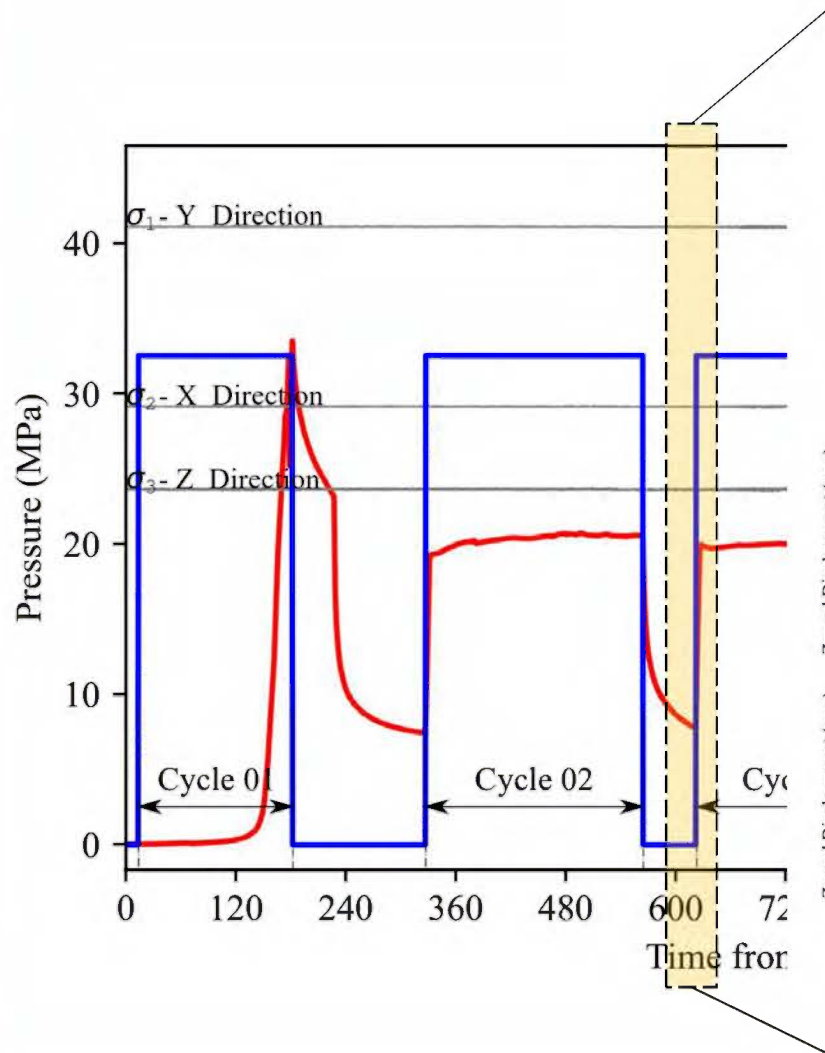




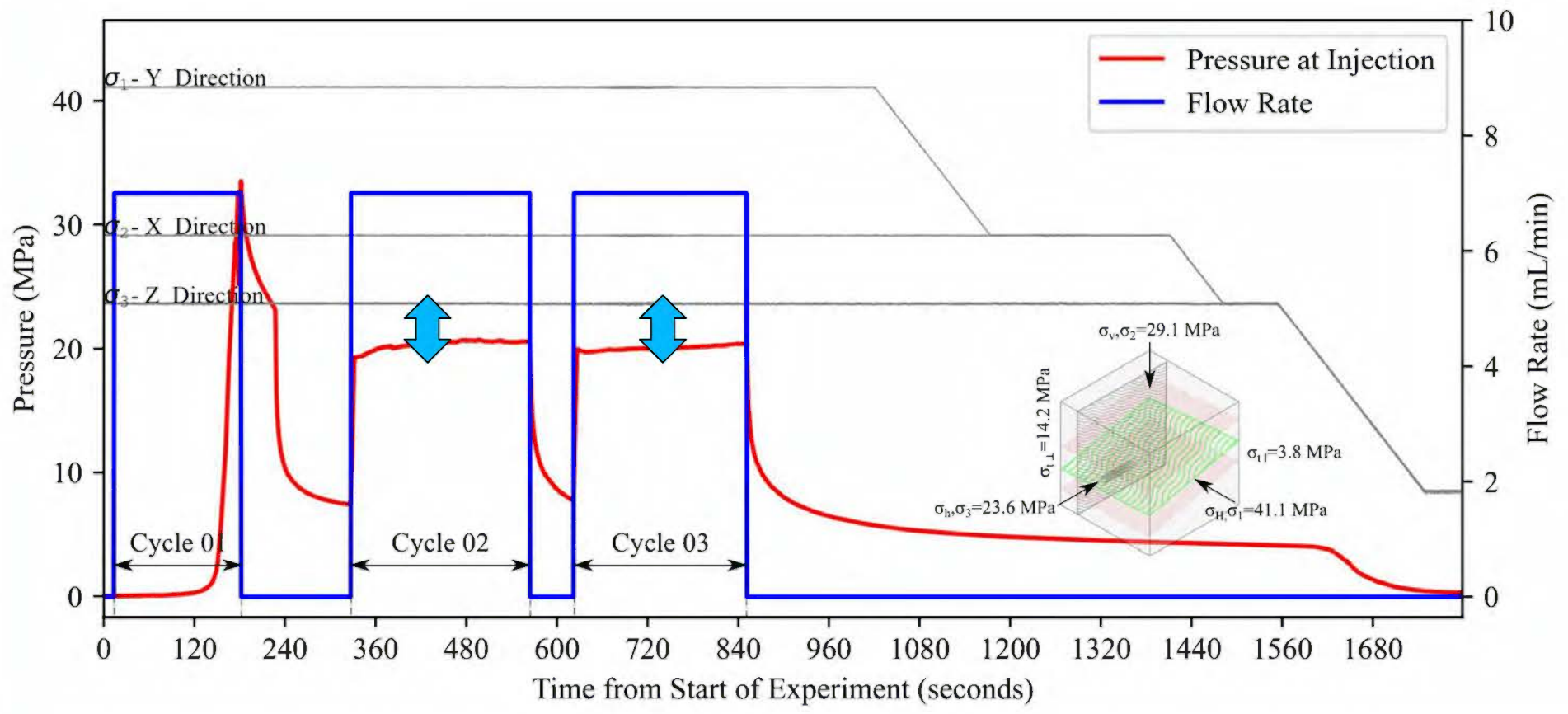
Sample B2-01 – Low Viscosity



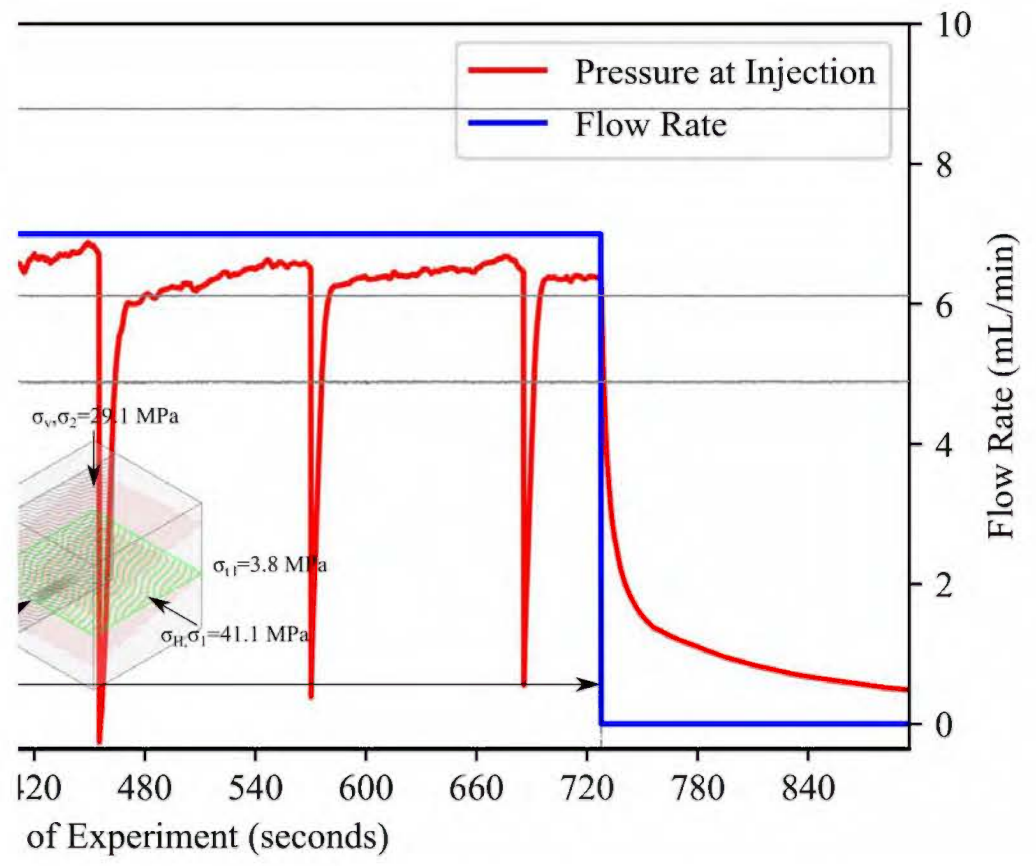
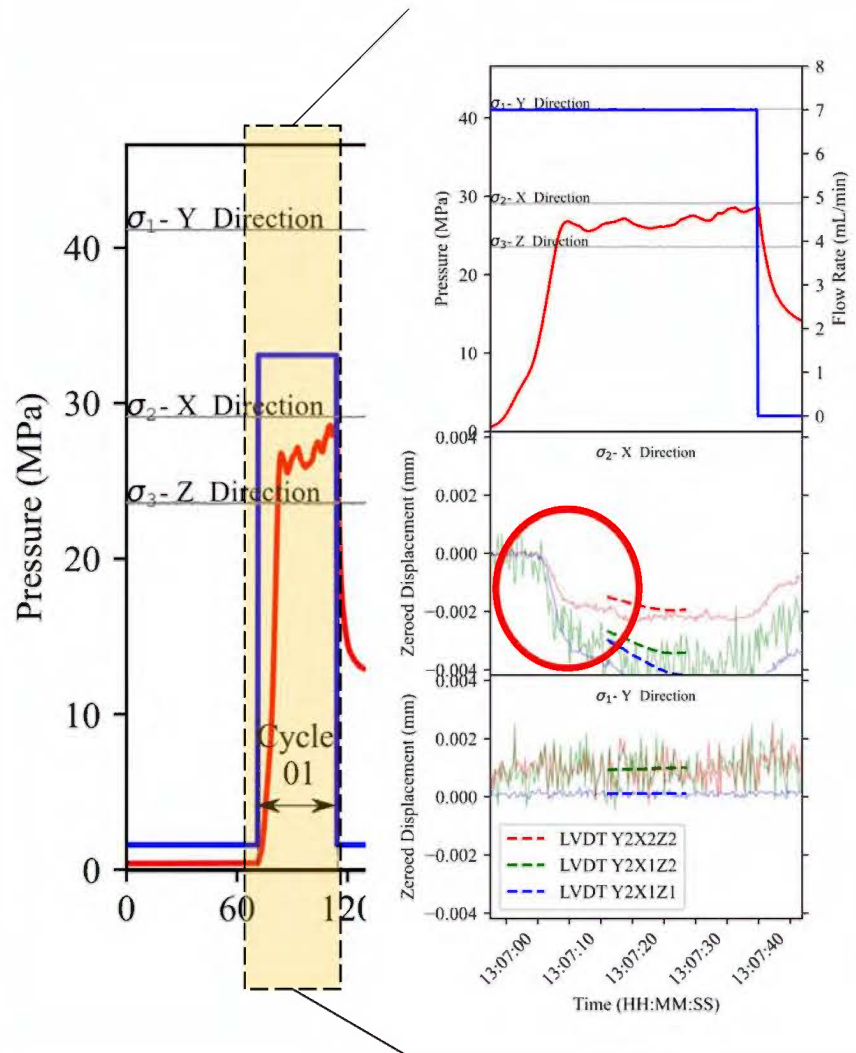
Sample B2-01 – Low Viscosity



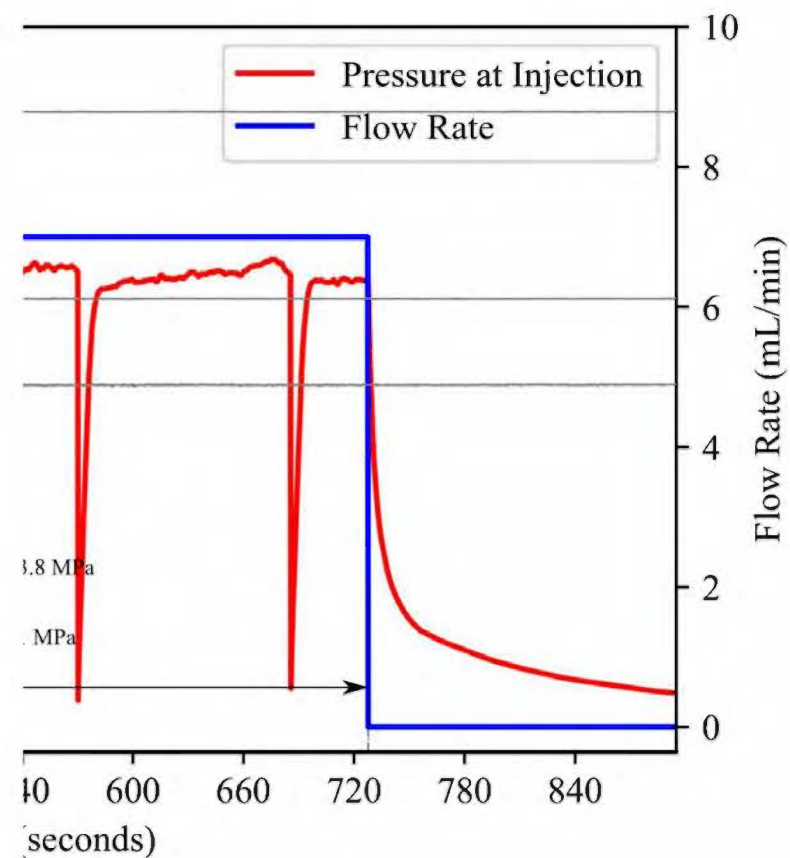
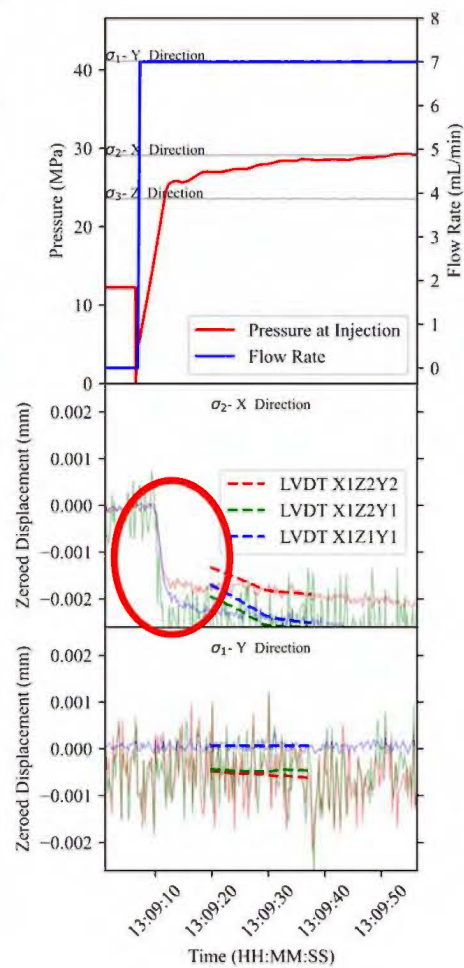
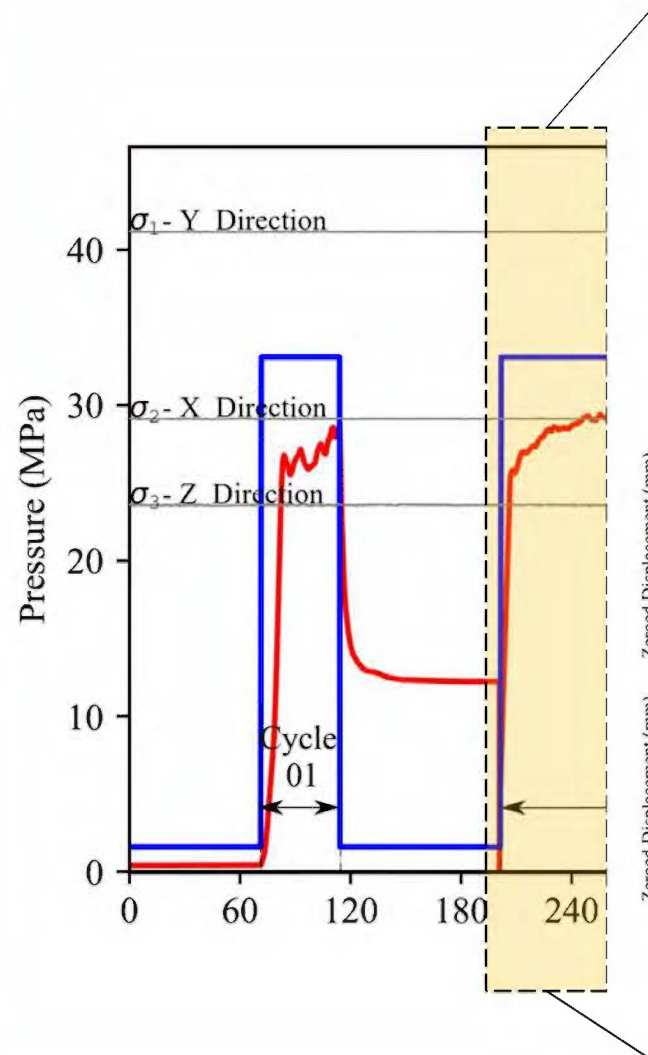
Sample B2-01 – Low Viscosity



Sample B2-01 – Low Viscosity

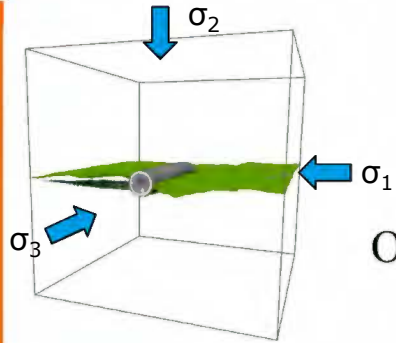


Sample B2-02 – High Viscosity

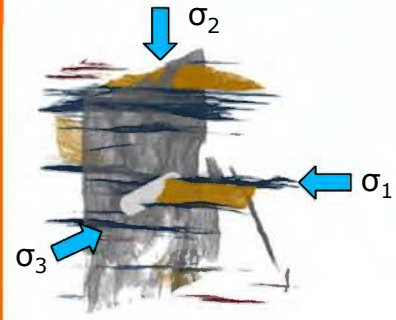


Sample B2-02 – High Viscosity

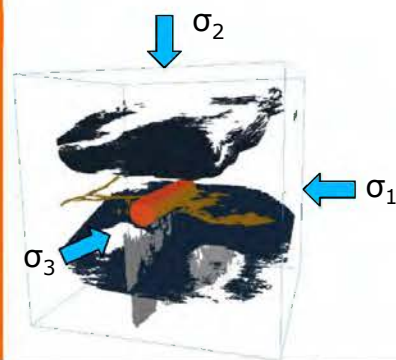
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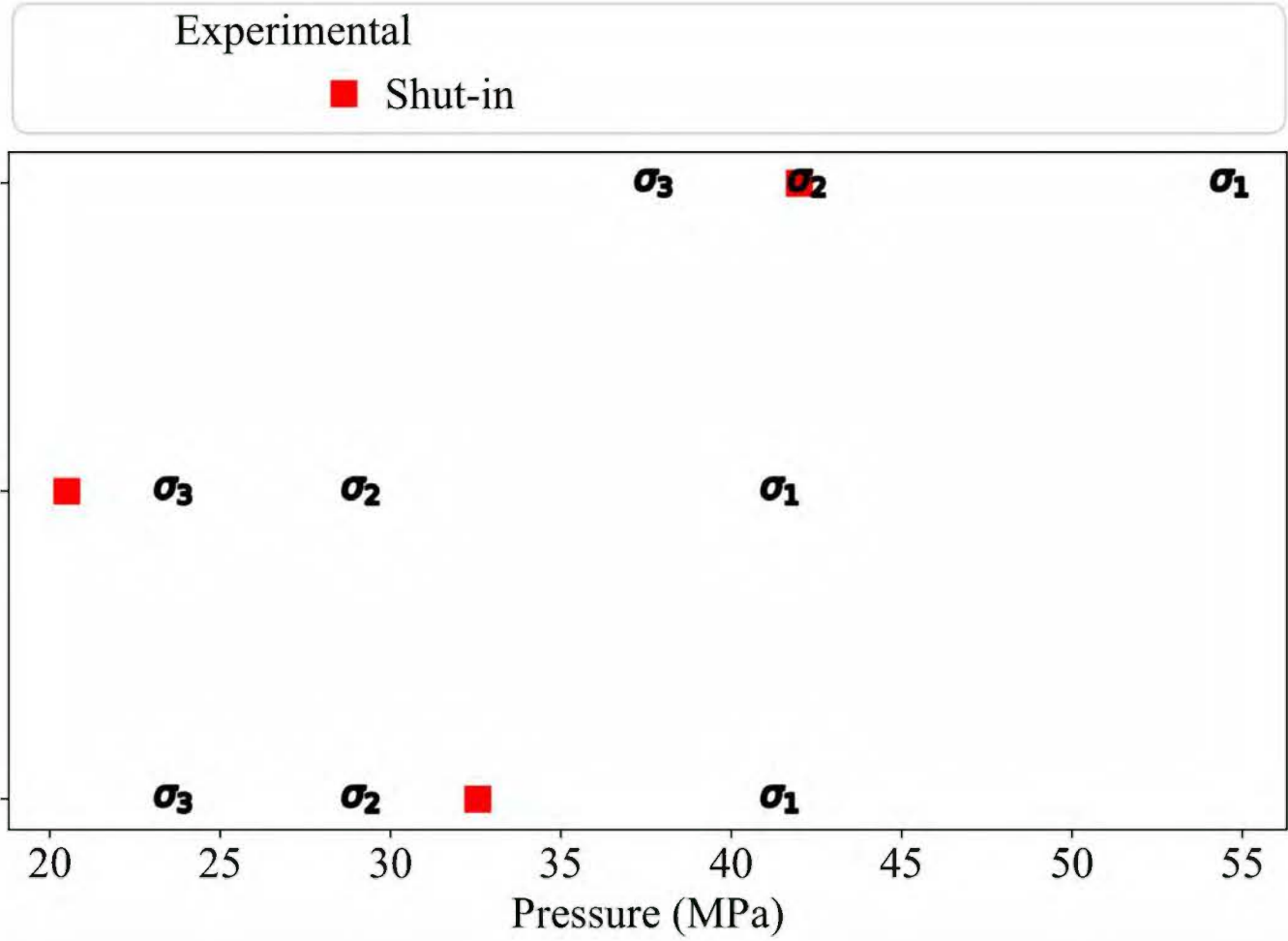
Outcrop 01



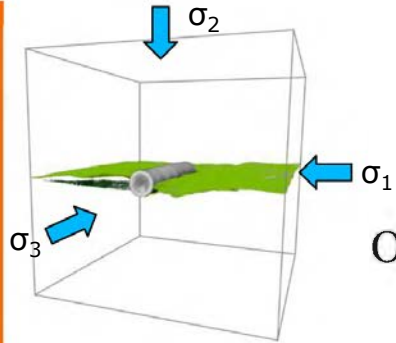
B2-01



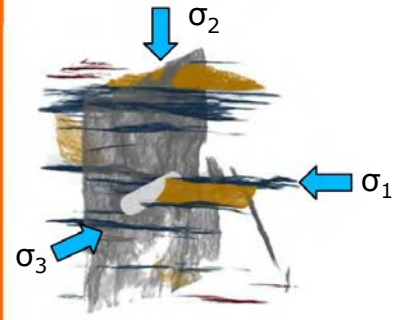
B2-02



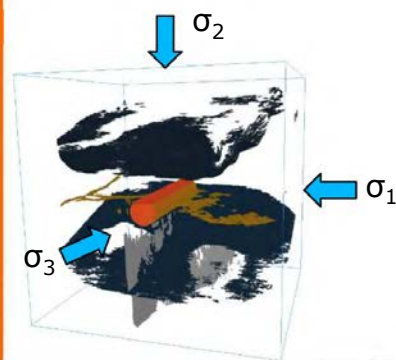
Comparison of Results – Shut-in



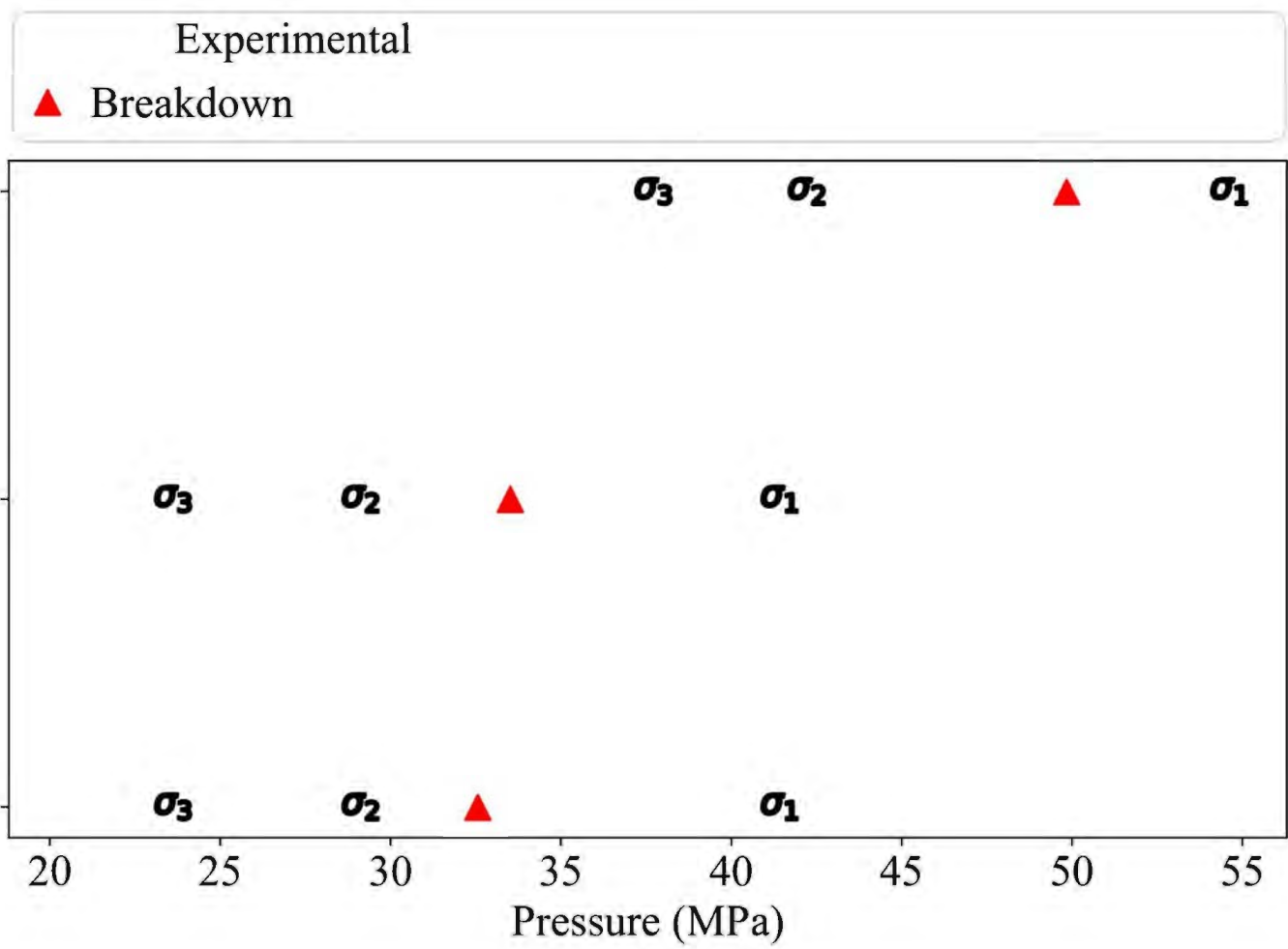
Outcrop 01



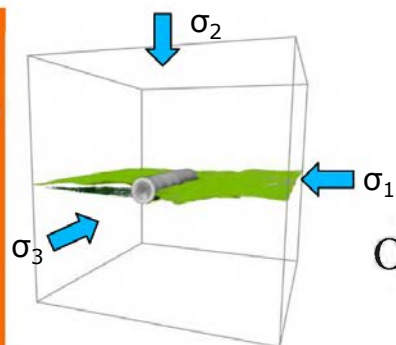
B2-01



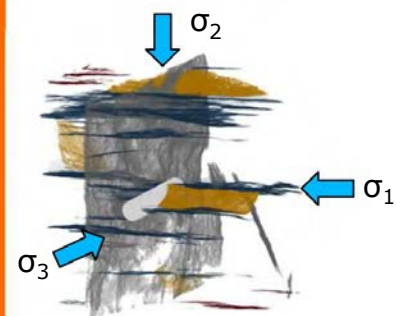
B2-02



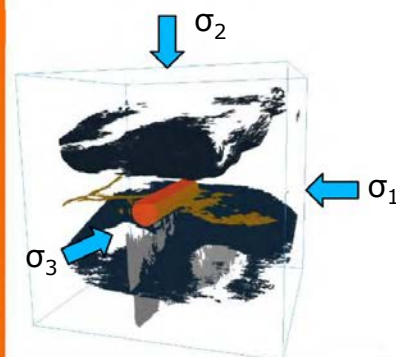
Comparison of Results – Breakdown



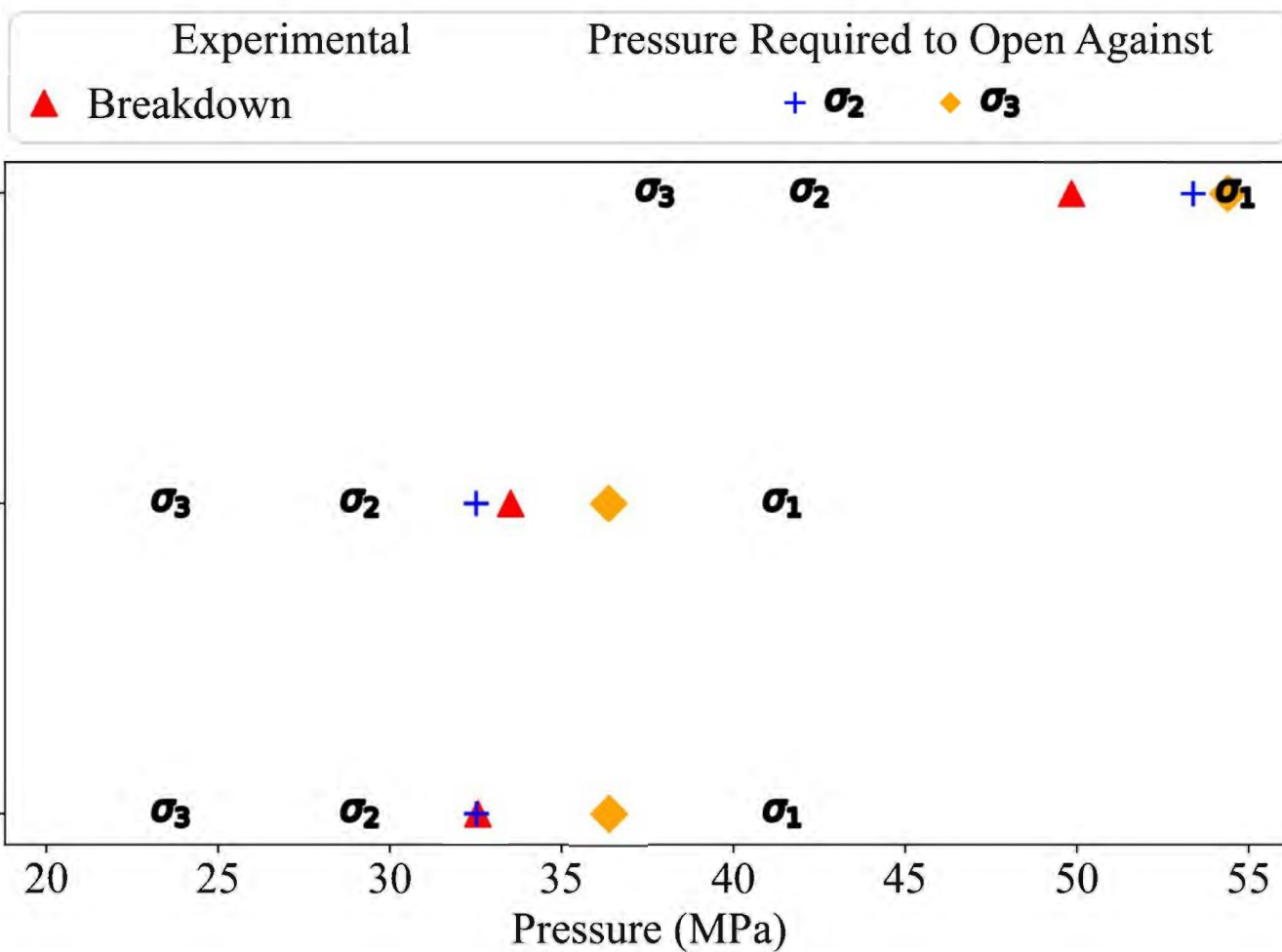
Outcrop 01



B2-01



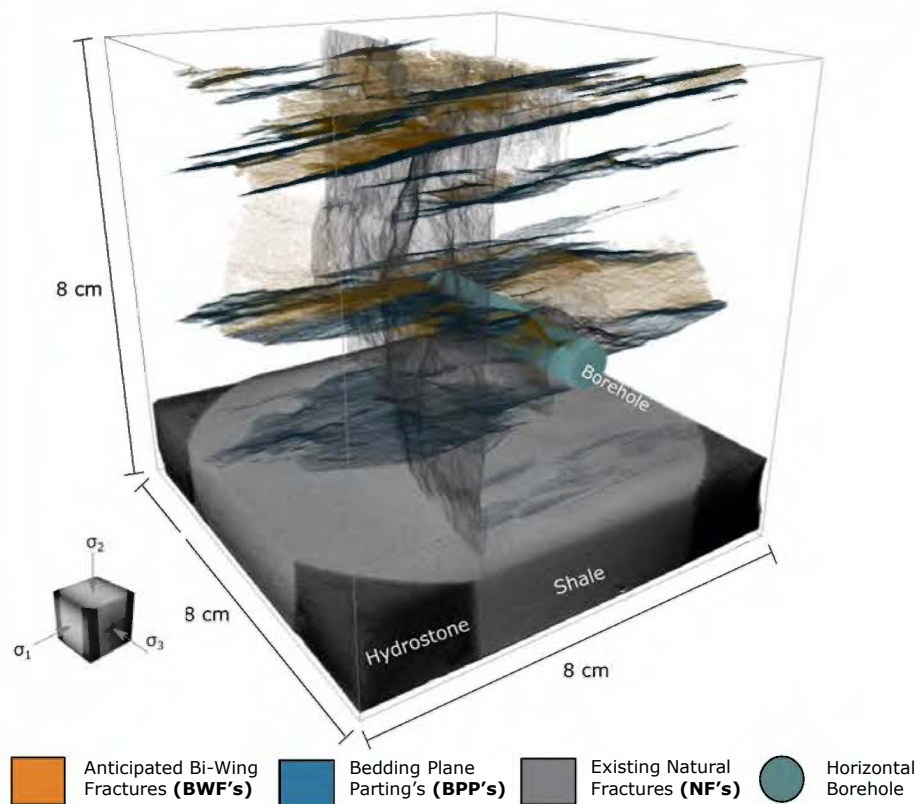
B2-02



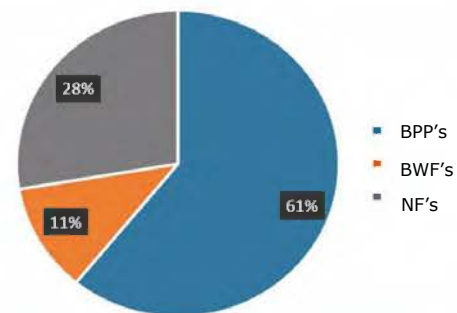
Comparison of Results – Breakdown Model

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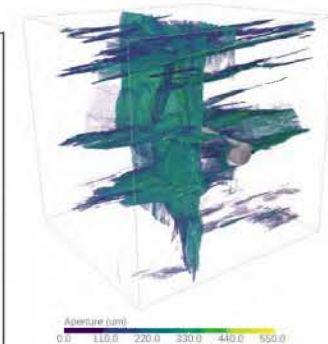
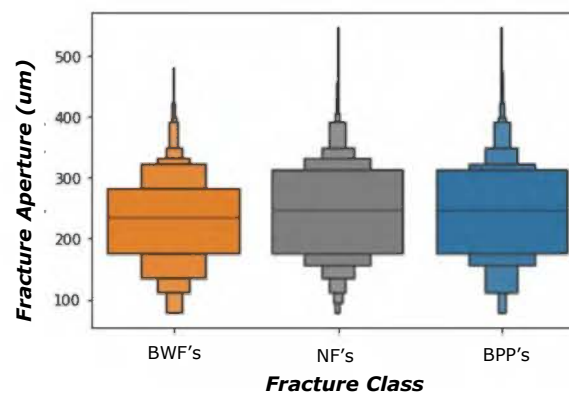
SRV Cube



Fracture Class Volume

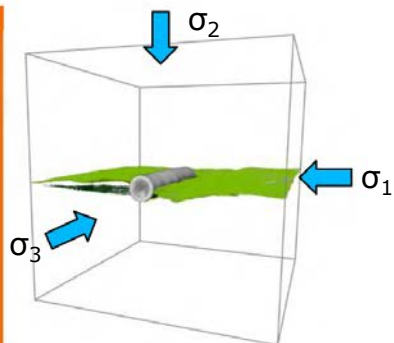


Aperture of Each Fracture Set



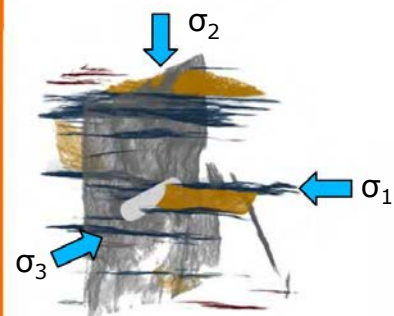
The majority of the Stimulated Rock Volume (SRV) is dominated by bedding plane partings, while bi-wing fractures have smaller aperture and volume, connecting the SRV

Fracture Geometry is Complex

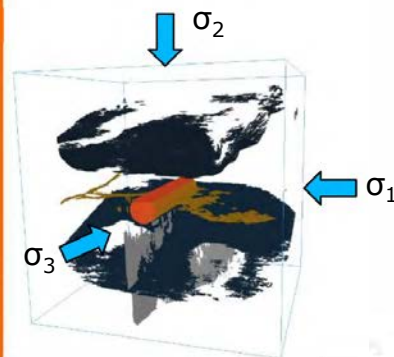


- Proposed a breakdown model that captures the in-situ stress contrast and the rock strength anisotropy:

$$P_b = \min(\sigma_{\text{in-situ}(\theta)} + \sigma_t(\theta)) - P_o ; \text{ when } \min(\sigma_{\text{in-situ}(\theta)} + \sigma_t(\theta)) < \sigma_\theta$$



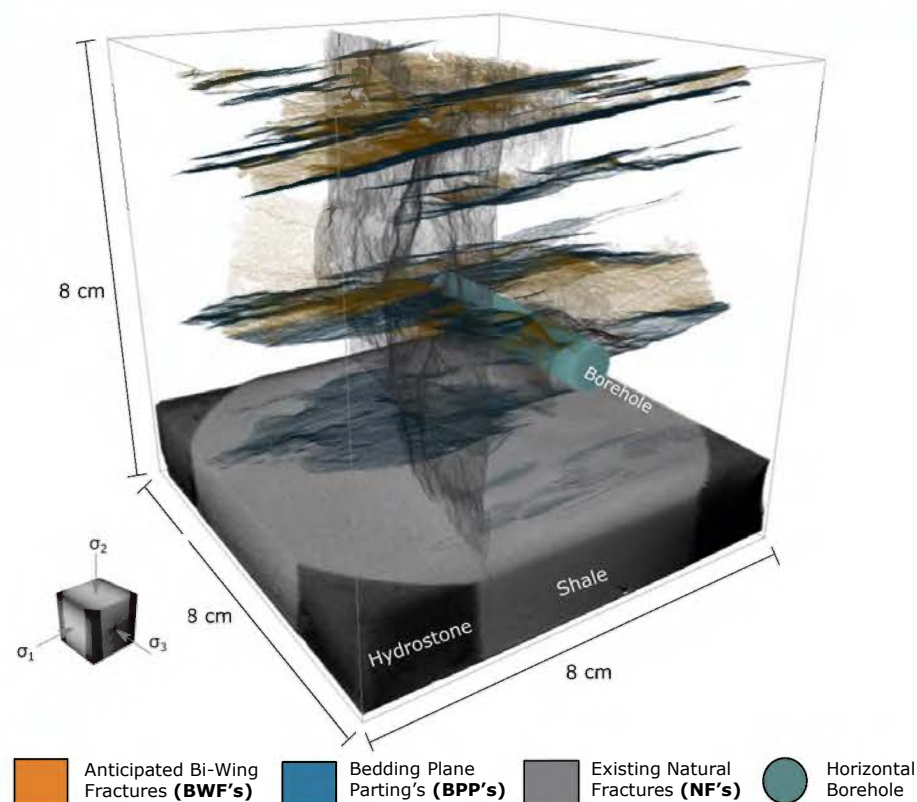
- Unique breakdown signature.
 - Tensile shows an abrupt change in the strain response that initiations before breakdown.
 - There is a lag in the abrupt change when using high viscosity fluids.
 - The strain response is very subtle during shear.



- The shut-in pressure can be used as a proxy to determine the complexity of the fracture. Planar fracture will usually resolve to the magnitude of a principal stress.
- High viscosity** leads to a hydraulic fracture and limits interaction with pre-existing weakness and discontinuities.

- While this experiment can be a proxy for near wellbore behaviour and tortuosity, it highly the significant role that strength anisotropy plays in dictating the fracture trajectory.
- Although acoustic emissions (AE) were monitored, there has been limited findings till date.
- The influence of pore-pressure was not addressed in this work.

SRV Cube



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